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TRAFFIC FLOW SIMULATION THROUGH SUCCESSIVE TRAFFIC SIGNALS



W.R. BELLIS

**DIRECTOR OF RESEARCH, TRANSPORTATION
NEW JERSEY DEPARTMENT OF TRANSPORTATION**



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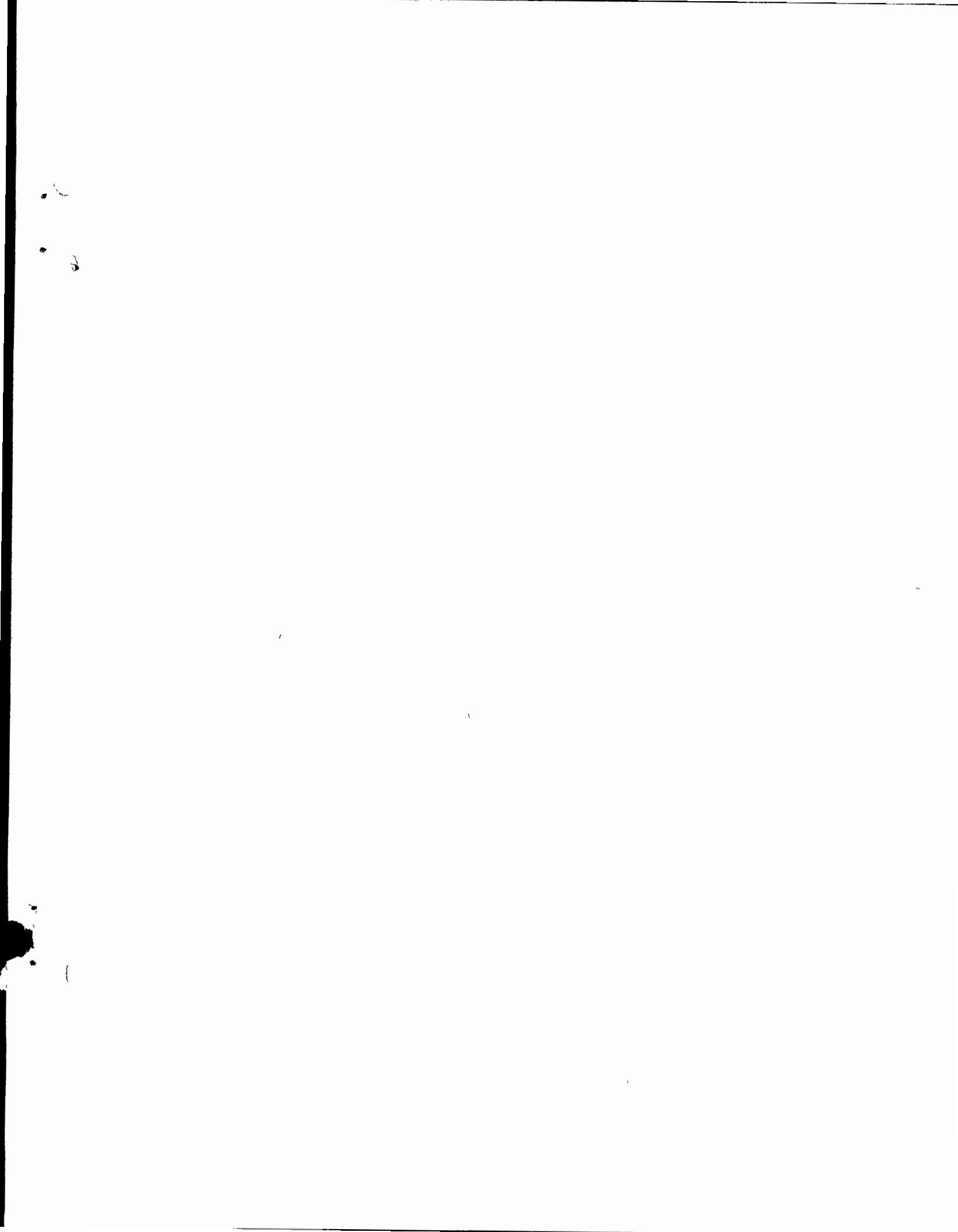
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ABSTRACT

TRAVEL TIME THROUGH SUCCESSIVE TRAFFIC SIGNALS BY A MATHEMATICAL PROCEDURE,
W. R. BELLIS, Director of Research, N. J. Department of Transportation,
1035 Parkway Avenue, Trenton, New Jersey

This paper describes in detail a mathematical procedure measuring the travel time in each direction through a series of traffic signals considering the following variables: (1) number of signalized locations, (2) the spacing of these locations, (3) the timing of each signal, (4) the offset of each signal, (5) the speed of vehicles, (6) the acceleration characteristics of vehicles, and (7) the volume of traffic. For a given set of signalized locations, all of these variables are fixed; then, by varying offsets, calculations will determine the travel time through the system for the average car in both directions. By testing all possible variations of offsets, the set producing the minimum travel time for both directions can be had. There was a very close agreement between a field test and calculations through a nine-mile section with 29 signals having spacings varying from 270 to 9,000 feet. Although this procedure is mathematically sound, we have not been able to examine it for minimum travel time. It is quite possible that others may be able to supply the missing link so that the set of offsets can be selected producing the least travel time. Without this, it is always possible that another set of offsets may produce a shorter travel time.



TRAFFIC FLOW SIMULATION THROUGH
SUCCESSIVE TRAFFIC SIGNALS

WHERE THERE IS A SYSTEM OF SUCCESSIVE SIGNALS ALONG A ROUTE IT IS VERY DESIRABLE TO SET THE OFFSETS SO AS TO PRODUCE THE MINIMUM TIME DELAY FOR THE TOTAL TWO WAY TRAFFIC. THE APPLICATION OF EXISTING PRACTICES IN SETTING UP TIME SPACE DIAGRAMMS DOES NOT NECESSARILY PRODUCE THE MINIMUM TRAVEL TIME. VERY OFTEN A RANDOM TRIAL SET OF OFFSETS MAY PRODUCE LESS TRAVEL TIME THAN A STANDARD SET OF OFFSETS AND THEN BY FURTHER TRIAL ANOTHER SET OF OFFSETS MAY PRODUCE A STILL SMALLER TRAVEL TIME. THE PROCEDURE FOR FINDING THE BEST OFFSETS HAS NOT YET BEEN DETERMINED OTHER THAN BY ACCIDENTAL TRIAL.

IT SEEMS REASONABLE THAT AN ALGEBRAIC EXPRESSION INCLUDING ALL THE VARIABLES COULD BE WRITTEN WHICH WOULD LEND ITSELF TO EXAMINATION FOR MAXIMUM AND MINIMUM TRAVEL TIME. SO FAR THIS HAS NOT BEEN DONE.

THIS REPORT DESCRIBES A MATHEMATICAL PROCEDURE BY MEANS OF WHICH THE TWO WAY TRAVEL TIME CAN BE DETERMINED FOR ANY SET OF GIVEN VARIABLES. THESE VARIABLES ARE:

1. NUMBER OF SIGNALIZED LOCATIONS
2. SPACING OF LOCATIONS
3. TIMING OF SIGNALS
4. SYNCHRONIZATION OF SIGNALS
5. ACCELERATION OF VEHICLES
6. SPEED OF VEHICLES
7. VOLUME OF TRAFFIC

A FIELD CHECK WAS MADE ALONG ROUTE US 1 FROM WOODBRIDGE TO ELIZABETH, NEW JERSEY THROUGH 28 SUCCESSIVE SIGNALS IN 8 MILES. THE AGREEMENT WAS VERY GOOD.

NOMENCLATURE - BY STEPS

STEP 1

- C = THE CYCLE LENGTH
- G = THE "GO" PHASE. THIS EQUALS THE GREEN PHASE PLUS A SMALL INTERVAL. THREE SECONDS IS USED HEREIN FOR THIS SMALL INTERVAL.
- N = THE NUMBER OF CARS APPROACHING THE SYSTEM DURING ONE CYCLE. THESE CARS APPROACH AT RANDOM SPACING BUT AVERAGE SPACING IS USED. THIS SEEMS JUSTIFIED SINCE MANY RANDOM SAMPLES WILL GIVE AVERAGE SPACING AS REPRESENTATIVE.
- $\alpha_0 D_1$ = THE CARS ORIGINATING AT ZERO (RANDOM) THAT ARE DELAYED AT LOCATION 1.
- α = THE TIME INTERVAL BETWEEN THE TIME THAT A STOPPED CAR PASSES A LOCATION AND THE TIME THAT THE SIGNAL AT THAT LOCATION TURNED GREEN. A CAR HAS PASSED A LOCATION WHEN THAT CAR HAS PASSED A POINT WHICH IS 50 FEET BEYOND THE STOP LINE WHERE THE STOP LINE IS REASONABLY PLACED, OTHERWISE WHERE THE STOP LINE SHOULD BE.
- α^1 = THE ALPHA OF THE 1ST STOPPED CAR.
- α^2 = THE ALPHA OF THE 2ND STOPPED CAR, ETC.

TABLE OF ALPHAS

$\alpha^1 = 5 \text{ Sec.}$	$\alpha^5 = 14 \text{ Sec.}$	$\alpha^9 = 22 \text{ Sec.}$
$\alpha^2 = 8 \text{ Sec.}$	$\alpha^6 = 16 \text{ Sec.}$	$\alpha^{10} = 24 \text{ Sec.}$
$\alpha^3 = 10 \text{ Sec.}$	$\alpha^7 = 18 \text{ Sec.}$	$\alpha^{11} = 25.75 \text{ Sec.}$
$\alpha^4 = 12 \text{ Sec.}$	$\alpha^8 = 20 \text{ Sec.}$	THEN ADD 1.75 SEC. PER CAR.

NOTE: FOR THIS STUDY ALL CYCLES ARE IDENTICAL.

$<$ = "LESS THAN". USE THE LARGEST VALUE WHICH IS "LESS THAN".
NOTE: A PART CAR CANNOT BE USED. USE THE WHOLE NUMBER WHICH IS LESS THAN THE FRACTION.

STEP 2

H_1 = THE TIME INTERVAL BETWEEN THE PASSING OF THE NTH CAR AND THE BEGINNING OF THE GREEN PHASE AT LOCATION 1.

STEP 3

oL_1 = THE UNDELAYED CARS FROM 0 TO LOCATION 1.
NOTE: ALL ELEMENTS AT LOCATION 1 OTHER THAN oD_1 , H_1 AND oL_1 ARE EQUAL TO ZERO.

STEP 4

\leq = EQUAL TO OR GREATER THAN THE VALUE TO WHICH IT POINTS.
 F_u = THE OFFSET AT LOCATION U. THE OFFSET IS THE BEGINNING OF THE GREEN PHASE DURING WHICH THE NTH CAR PASSES.
 $U-1$ = THE LOCATION BACK OF LOCATION U. READ AS THE LOCATION U MINUS ONE.
 $u-1e_u$ = THE TRAVEL TIME FROM LOCATION U-1 TO LOCATION U AT NORMAL SPEED NOT INCLUDING ACCELERATION AND DECELERATION.
 U = ANY SIGNALIZED LOCATION EXCEPT LOCATION 1.
 F'_u = THE BASIC STATED F_u . IT IS GENERALLY GIVEN AS THE ONE LESS THAN C GREATER THAN ZERO.
 M = A MULTIPLE OF - - .

STEP 5

W = ANY LOCATION 1 TO U-1 AS AN ORIGINATING POINT.
 V = EACH AND EVERY LOCATION BETWEEN W AND U.

NOTE: WHEN oL_{u-1} TO $P_{u-1} = 0$
THEN oL_u , oD_u , oD_u , $oP_u = 0$
AND WHEN $wL_{u-1} + wP_{u-1} = 0$
THEN wL_u , wD_u , wD_u , $wP_u = 0$

$\acute{w}D\bar{v}$ = THE CARS ORIGINATING AT W DURING THE G FOLLOWING F_w (BY THE PRIME AT THE UPPER LEFT) WHICH ARE DELAYED AT V AND PASS V DURING THE G WHICH FOLLOWS F_v (BY THE D) AFTER HAVING BEEN DELAYED AT V BY CARS WHICH PASSED W DURING THE G PRECEDING F_w (BY THE DOUBLE BAR AT THE UPPER RIGHT).

$\acute{w}dv$ = THE CARS ORIGINATING AT W DURING THE G WHICH FOLLOWS F_w (BY THE PRIME AT THE UPPER LEFT) WHICH ARE DELAYED AT V AND PASS V DURING THE G WHICH PRECEDES F_v (BY THE SMALL d).

F_w = THE OFFSET AT W.

$\acute{w}Pu$ = THE CARS WHICH ORIGINATE AT W DURING THE G WHICH FOLLOWS F_w AND THEN PASS U DURING THE G WHICH PRECEDES F_u .

NOTE: A SINGLE PRIME INDICATES PASSAGE DURING THE G FOLLOWING F AND A DOUBLE PRIME INDICATES PASSAGE DURING THE G PRECEDING F. WHEN AN ATTACHMENT IS OMITTED IT INDICATES THAT ALL POSSIBLE APPLICATIONS ARE TO BE USED.

$\acute{w}Lu-1$ = THE CARS WHICH ORIGINATE AT W DURING THE G FOLLOWING F_w AND PASS UNDELAYED AT U-1 DURING EITHER THE G WHICH FOLLOWS OR PRECEDES F_u-1 (BY THE OMISSION OF THE PRIMES).

NOTE: THE \leq (EQUAL TO OR LESS THAN) IS USED TO INDICATE THAT WHERE MORE THAN ONE RESULT IS POSSIBLE FROM THE PROCEDURE THE SMALLER (SMALLEST) VALUE IS USED.

$\acute{w}Lw$ = D_w

NOTE: WHEN $\bar{w}Lu-1 = 0$ then $\bar{w}Lu = 0$.

STEP 6

$\acute{\acute{w}}Lw$ = dw

STEP 7

$\frac{1}{w\bar{d}u}$ = THE $\acute{w}du$ CARS WHICH INCLUDE THE FIRST CAR OF THE n CARS AT w AND ALSO AT u . THE SINGLE BAR INDICATES THAT THE FIRST CAR IS INCLUDED IN THE GROUP.

$\bar{w}Lu-1$ = THE $wLu-1$ CARS WHICH INCLUDE THE FIRST CAR.

STEP 9

$\frac{1}{w\hat{d}u}$ = THE $\acute{w}du$ CARS WHICH AT u MAY OR MAY NOT INCLUDE THE FIRST CAR.

STEP 11

$o\hat{p}u$ = THE SECOND GROUP OF oPu CARS WHEN THERE ARE TWO GROUPS OF CARS FROM o PASSING u DURING THE G PRECEDING Fu .

$o\hat{L}u-1$ = THE SECOND GROUP OF UNDELAYED CARS FROM o TO $u-1$ WHEN THERE ARE TWO GROUPS PASSING $u-1$ DURING THE G PRECEDING $Fu-1$.

$o\overset{\curvearrowright}{L}u-1$ = THE FIRST GROUP OF UNDELAYED CARS WHEN THERE ARE TWO GROUPS FROM o TO $u-1$ PASSING $u-1$ DURING THE G PRECEDING $Fu-1$.

$o\overset{<}{L}u-1$ = THE $oLu-1$ CARS PASSING $u-1$ DURING THE G PRECEDING $Fu-1$ WHEN THERE IS ONLY ONE GROUP OF UNDELAYED CARS FROM o TO $u-1$.

STEP 12

$o\overset{\curvearrowright}{p}u$ = THE FIRST GROUP OF CARS WHEN THERE ARE TWO GROUPS FROM o TO u PASSING u DURING THE G PRECEDING Fu .

STEP 13

$o\overset{<}{p}u$ = THE CARS FROM o PASSING u DURING THE G PRECEDING u WHEN THERE IS ONLY ONE GROUP OF CARS FROM o TO u PASSING u DURING THE G PRECEDING Fu .

STEP 14

Qu = THE TOTAL CARS PASSING DURING THE G PRECEDING Fu .

STEP 15

$\acute{w}\bar{D}_u$ = THE $\acute{w}D_u$ CARS DELAYED AT U BY CARS WHICH PASSED W DURING THE G WHICH PRECEDES Fw.

STEP 16

$\acute{w}D_u^{\square}$ = THE $\acute{w}D_u$ CARS WHICH ARE DELAYED AT U DIRECTLY BY (C - G) INCLUDING THE $\frac{1}{w}\bar{D}_u$ AND $\frac{1}{w}D_u^{\Delta}$ CARS.

STEP 17

oD_u° = THE oD_u CARS WHICH WERE $oL_u^{\circ}-1$ CARS.

STEP 18

oD_u^{\wedge} = THE oD_u CARS WHICH WERE $oL_u^{\wedge}-1$ CARS.

STEP 19

oD_u^{\lessdot} = THE oD_u CARS WHICH WERE $oL_u^{\lessdot}-1$ CARS.

STEP 20

$oD_u^{\acute{}}$ = THE oD_u CARS WHICH WERE $oL_u^{\acute{}}-1$ CARS.

STEP 34

$\overset{\circ}{o}L_x^{\lessdot}$ = THE oL_x^{\lessdot} CARS WHICH WERE $oL_x^{\lessdot}-1$ OR $oL_x^{\circ}-1$ CARS.

STEP 35

$\hat{o}L_x^{\lessdot}$ = THE oL_x^{\lessdot} CARS WHICH WERE $oL_x^{\lessdot}-1$ OR $oL_x^{\wedge}-1$ CARS.

STEP 36

$\acute{w}L_x^N$ = THOSE wL_x CARS WHICH INCLUDE THE N^{th} CAR.

STEP 37

$\frac{t}{\overset{\circ}{o}L_x}$ = THE SUMMATION OF THE TIMES OF ALL oL_x° CARS IN PASSING X.

$\frac{t}{\hat{o}L_x}$ = THE SUMMATION OF THE TIMES OF ALL oL_x^{\wedge} CARS IN PASSING X.

STEP 38

t_1 = THE SUM OF ALL THE N CARS AS THEY ARE DUE TO ARRIVE AT
LOCATION 1 ASSUMING THAT THEY WOULD NOT STOP.

STEP 39

t_x = THE TIME TO TRAVEL FROM 1 THROUGH X WITH THE GIVEN SIGNAL
SYSTEM.

STEP 40

t_x = THE TIME LOSS BECAUSE OF THE GIVEN SIGNAL SYSTEM COMPARED
TO TRAVELING THE DISTANCE AT NORMAL UNIFORM UNINTERRUPTED
SPEED.

STEP 1

$$\frac{C}{N} (oD_1) - \alpha \frac{oD_1}{2N} < (C - G) + \frac{C}{2N}$$

SOLVE FOR oD_1

IN FIG. 1-1

$$\frac{C}{N} (oD_1) - \frac{C}{2N} - (C - G) < \alpha \frac{oD_1}{2N} \quad \text{OR TRANSPOSING}$$

$$\frac{C}{N} (oD_1) - \alpha \frac{oD_1}{2N} < (C - G) + \frac{C}{2N}$$

STEP 2

$$H_1 = \left(\begin{array}{l} \alpha \frac{oD_1}{2N} \\ G - \frac{C}{2N} \end{array} \right) \text{ OR } \left. \begin{array}{l} \\ \end{array} \right\} \text{ USE LARGER}$$

SOLVE FOR H_1

IN FIG. 2-1

$$H_1 = \alpha \frac{oD_1}{2N} \text{ WHICH IS LARGER THAN } G - \frac{C}{2N}$$

IN FIG. 2-2

$$H_1 = G - \frac{C}{2N} \text{ WHICH IS LARGER THAN } \alpha \frac{oD_1}{2N}$$

THESE TWO FIGURES ILLUSTRATE ALL POSSIBILITIES
OF VARIATION OF H_1 .

STEP 3

$$oL_j' = N - oD_1$$

ALL ELEMENTS TO LOCATION 1 OTHER THAN

oD_1 , H_1 AND oL_1' ARE EQUAL TO ZERO.

SOLVE FOR

$$oL_1'$$

FIG. 1-1

GIVEN $N = 6$ $oD_1 = 3$

$$oL_1' = 6 - 3 = 3$$

STEP 4

$$F_u \Rightarrow F_{u-1} + H_{u-1} + u-1 C_u - G \quad \text{AND}$$

$$F_u < F_{u-1} + H_{u-1} + u-1 C_u - G + C \quad \text{BUT}$$

$$F_u = F_u' + MC$$

SOLVE FOR F_u

F_u MAY VARY THROUGH A TIME LENGTH OF ONE CYCLE. THE ABOVE LIMITS ARE ARBITRARILY SELECTED BUT THE SELECTION WAS INFLUENCED BY A DESIRE TO SIMPLIFY THE SOLUTION OF THE OVERALL PROBLEM.

IN FIG. 4-1 AND 4-2

F_u IS PLOTTED AT THE LOWEST POSSIBLE POINT. IF IT WERE PLOTTED LOWER THEN THE Nth CAR WOULD NOT PASS DURING THE GREEN PHASE FOLLOWING F_u . F_u MAY VARY UP TO $F_u + C$ BUT NOT EQUAL TO $F_u + C$. IF $F_u = F_u + C$ THEN THE Nth CAR DOES NOT PASS F_u DURING THE GREEN PHASE FOLLOWING F_u .

STEP 5

$$\alpha \frac{\hat{w}D\bar{v} + \hat{w}dv + \hat{w}Pu}{\hat{w}Pu} \leq Fu - Fw - wCu - (C - G) \quad \text{AND}$$

$$\hat{w}Pu \leq \hat{w}Lu-i \quad \text{BUT WHEN}$$

$$Fw + \alpha_i + wCu \geq Fu - (C-G) \quad \text{THEN}$$

$$\hat{w}Pu = 0$$

SOLVE FOR $\hat{w}Pu$

UNDER SOME CONDITIONS THE 1ST PART WILL GIVE VALUES GREATER THAN TRUE VALUES; IN SUCH CASES THE 2ND PART WILL GIVE THE TRUE VALUE.

IN ALL FIGURES

$$Fw + \alpha \frac{\hat{w}D\bar{v} + \hat{w}dv + \hat{w}Pu}{\hat{w}Pu} + wCu \leq Fu - (C - G)$$

WHICH WHEN TRANSPOSED GIVES THE FIRST PART OF THE STEP.

EXAMPLES:

FIG. 5-1

Given $\hat{w}D\bar{v} = 0$ $\hat{w}dv = 0$ $Fu = 121$

$Fw = 70$ $wCu = 8$ $(C - G) = 30$ $\hat{w}Lu-i = 5$

$$\alpha \frac{0 + 0 + \hat{w}Pu}{\hat{w}Pu} \leq 121 - 70 - 8 - 30$$

$$\alpha \frac{\hat{w}Pu}{\hat{w}Pu} \leq 13$$

$$\hat{w}Pu \leq \begin{pmatrix} 4 \\ 5 \end{pmatrix} \begin{matrix} + \text{1ST PART} \\ + \text{2ND PART} \end{matrix}$$

FIG. 5-2

Given $\hat{w}D\bar{v} = 0$ $\hat{w}dv = 0$ $Fu = 140$

$Fw = 70$ $wCu = 8$ $(C - G) = 30$ $\hat{w}Lu-i = 7$

$$\alpha \frac{0 + 0 + \hat{w}Pu}{\hat{w}Pu} \leq 140 - 70 - 8 - 30$$

$$\alpha \frac{\hat{w}Pu}{\hat{w}Pu} \leq 32$$

$$\hat{w}Pu \leq \begin{pmatrix} 14 \\ 7 \end{pmatrix} \begin{matrix} \text{1ST} \\ + \text{2ND} \end{matrix}$$

FIG. 5-3

$$\begin{aligned} \text{Given } \hat{w}D\bar{v} &= 0 & \hat{w}dv &= 0 & F_u &= 120 \\ F_w &= 75 & wC_u &= 8 & (C - G) &= 30 & \hat{w}Lu-l &= 5 \\ \alpha \frac{0 + 0 + \hat{w}Pu}{\hat{w}Pu} & & & & \leq & 120 - 75 - 8 - 30 \\ \alpha \frac{\hat{w}Pu}{\hat{w}Pu} & & & & \leq & 7 \\ \hat{w}Pu & & & & \leq & \begin{pmatrix} 1 & \text{1ST} \\ 5 & \text{2ND} \end{pmatrix} \end{aligned}$$

FIG. 5-4

$$\begin{aligned} \text{Given } \hat{w}D\bar{v} &= 0 & \hat{w}dv &= 0 & F_u &= 170 \\ F_w &= 70 & wC_u &= 8 & (C - G) &= 30 & \hat{w}Lu-l &= 7 \\ \alpha \frac{0 + 0 + \hat{w}Pu}{\hat{w}Pu} & & & & \leq & 170 - 70 - 8 - 30 \\ \alpha \frac{\hat{w}Pu}{\hat{w}Pu} & & & & \leq & 62 \\ \hat{w}Pu & & & & \leq & \begin{pmatrix} 31 & \text{1ST} \\ 7 & \text{2ND} \end{pmatrix} \end{aligned}$$

FIG. 5-5

$$\begin{aligned} \text{Given } \hat{w}D\bar{v} &= 0 & \hat{w}dv &= 0 & F_u &= 180 \\ F_w &= 60 & wC_u &= 10 & (C - G) &= 30 & \hat{w}Lu-l &= 7 \\ \alpha \frac{0 + 0 + \hat{w}Pu}{\hat{w}Pu} & & & & \leq & 180 - 60 - 10 - 30 \\ \alpha \frac{\hat{w}Pu}{\hat{w}Pu} & & & & \leq & 80 \\ \hat{w}Pu & & & & \leq & \begin{pmatrix} 42 & \text{1ST} \\ 7 & \text{2ND} \end{pmatrix} \end{aligned}$$

FIG. 5-6

$$\begin{aligned} \text{Given } \hat{w}D\bar{v} &= 0 & \hat{w}dv &= 0 & F_u &= 198 \\ F_w &= 75 & wC_u &= 11 & (C - G) &= 30 & \hat{w}Lu-l &= 3 \\ \alpha \frac{0 + 0 + \hat{w}Pu}{\hat{w}Pu} & & & & \leq & 198 - 75 - 11 - 30 \\ \alpha \frac{\hat{w}Pu}{\hat{w}Pu} & & & & \leq & 82 \\ \hat{w}Pu & & & & \leq & \begin{pmatrix} 43 & \text{1ST} \\ 3 & \text{2ND} \end{pmatrix} \end{aligned}$$

FIG. 5-7

$$\begin{aligned} \text{Given } \overline{wDv} &= 0 & \overline{wdv} &= 1 & F_u &= 115 \\ F_w &= 60 & wC_u &= 10 & (C - G) &= 30 & \overline{wLu-1} &= 6 \\ \alpha \frac{0 + 1 + \overline{wPu}}{1 + \overline{wPu}} & & & & \leq & 115 - 60 - 10 - 30 \\ \alpha \frac{1 + \overline{wPu}}{1 + \overline{wPu}} & & & & \leq & 15 \\ 1 + \overline{wPu} & & & & \leq & 5 \\ \overline{wPu} & & & & \leq & \begin{pmatrix} 4 & + & 1\text{ST} \\ 6 & & 2\text{ND} \end{pmatrix} \end{aligned}$$

FIG. 5-8

$$\begin{aligned} \text{Given } \overline{wDv} &= 1 & \overline{wdv} &= 0 & F_u &= 125 \\ F_w &= 74 & wC_u &= 8 & (C - G) &= 30 & \overline{wLu-1} &= 4 \\ \alpha \frac{1 + 0 + \overline{wPu}}{1 + \overline{wPu}} & & & & \leq & 125 - 74 - 8 - 30 \\ \alpha \frac{1 + \overline{wPu}}{1 + \overline{wPu}} & & & & \leq & 13 \\ 1 + \overline{wPu} & & & & \leq & 4 \\ \overline{wPu} & & & & \leq & \begin{pmatrix} 3 & + & 1\text{ST} \\ 4 & & 2\text{ND} \end{pmatrix} \end{aligned}$$

FIG. 5-9

$$\begin{aligned} \text{Given } \overline{wDv} &= 0 & \overline{wdv} &= 3 & F_u &= 155 \\ F_w &= 100 & wC_u &= 12 & (C - G) &= 30 & \overline{wLu-1} &= 1 \\ \alpha \frac{0 + 3 + \overline{wPu}}{3 + \overline{wPu}} & & & & \leq & 155 - 100 - 12 - 30 \\ \alpha \frac{3 + \overline{wPu}}{3 + \overline{wPu}} & & & & \leq & 13 \\ 3 + \overline{wPu} & & & & \leq & 4 \\ \overline{wPu} & & & & \leq & \begin{pmatrix} 1 & + & 1\text{ST} \\ 1 & + & 2\text{ND} \end{pmatrix} \end{aligned}$$

NOTE THAT SINCE V = EACH AND EVERY LOCATION BETWEEN
THE ORIGINATING POINT AND U; $\overline{wdv} = w_{d+1} + w_{d+2} + \dots$
 $\dots + w_{d-1}$

STEP 6

$$\alpha \frac{Dw + \overset{\prime\prime}{w}dv + \overset{\prime\prime}{w}Pu}{\overset{\prime\prime}{w}Pu} \leq Fu - Fw - wCu + G \quad \text{AND}$$

$$\leq \overset{\prime\prime}{w}Lu-1 \quad \text{AND WHEN}$$

$$dw = 0 \quad \text{THEN}$$

$$\overset{\prime\prime}{w}Pu = 0$$

SOLVE FOR $\overset{\prime\prime}{w}Pu$

IN ALL FIGURES

$$Fw - C + \alpha \frac{Dw + \overset{\prime\prime}{w}dv + \overset{\prime\prime}{w}Pu}{\overset{\prime\prime}{w}Pu} + wCu \leq Fu - (C - G)$$

EXAMPLES:

FIG. 6-1

Given $Dw = 1$ $\overset{\prime\prime}{w}dv = 0$ $Fu = 80$
 $Fw = 151$ $wCu = 10$ $G = 90$ $\overset{\prime\prime}{w}Lu-1 = 1$

$$\alpha \frac{1 + 0 + \overset{\prime\prime}{w}Pu}{1 + \overset{\prime\prime}{w}Pu} \leq 80 - 151 - 10 + 90$$

$$\frac{1 + \overset{\prime\prime}{w}Pu}{1 + \overset{\prime\prime}{w}Pu} \leq 9$$

$$1 + \overset{\prime\prime}{w}Pu \leq 2$$

$$\overset{\prime\prime}{w}Pu \leq \begin{matrix} (1 + 1\text{ST}) \\ (1 + 2\text{ND}) \end{matrix}$$

FIG. 6-2

Given $Dw = 1$ $\overset{\prime\prime}{w}dv = 0$ $Fu = 66$
 $Fw = 130$ $wCu = 11$ $G = 90$ $\overset{\prime\prime}{w}Lu-1 = 4$

$$\alpha \frac{1 + 0 + \overset{\prime\prime}{w}Pu}{1 + \overset{\prime\prime}{w}Pu} \leq 66 - 130 - 11 + 90$$

$$\frac{1 + \overset{\prime\prime}{w}Pu}{1 + \overset{\prime\prime}{w}Pu} \leq 15$$

$$1 + \overset{\prime\prime}{w}Pu \leq 5$$

$$\overset{\prime\prime}{w}Pu \leq \begin{matrix} (4 + 1\text{ST}) \\ (4 + 2\text{ND}) \end{matrix}$$

FIG. 6-3

$$\begin{aligned} \text{Given } D_w &= 1 \quad \ddot{w}_{dv} = 0 \quad F_u = 139 \\ F_w &= 130 \quad w_{Cu} = 11 \quad G = 90 \quad \ddot{w}_{Lu-1} = 4 \\ \alpha \frac{1 + 0 + \ddot{w}_{Pu}}{1 + \ddot{w}_{Pu}} &\leq 139 - 130 - 11 + 90 \\ \alpha \frac{1 + \ddot{w}_{Pu}}{1 + \ddot{w}_{Pu}} &\leq 88 \\ 1 + \ddot{w}_{Pu} &\leq 46 \\ \ddot{w}_{Pu} &\leq \begin{cases} 45 & \text{1ST} \\ 4 & \text{2ND} \end{cases} \end{aligned}$$

FIG. 6-4

$$\begin{aligned} \text{Given } D_w &= 3 \quad \ddot{w}_{dv} = 0 \quad F_u = 174 \\ F_w &= 170 \quad w_{Cu} = 7.5 \quad G = 90 \quad \ddot{w}_{Lu-1} = 7 \\ \alpha \frac{3 + 0 + \ddot{w}_{Pu}}{3 + \ddot{w}_{Pu}} &\leq 174 - 170 - 7.5 + 90 \\ \alpha \frac{3 + \ddot{w}_{Pu}}{3 + \ddot{w}_{Pu}} &\leq 86.5 \\ 3 + \ddot{w}_{Pu} &\leq 45 \\ \ddot{w}_{Pu} &\leq \begin{cases} 42 & \text{1ST} \\ 7 & \text{2ND} \end{cases} \end{aligned}$$

FIG. 6-5

$$\begin{aligned} \text{Given } D_w &= 3 \quad \ddot{w}_{dv} = 6 \quad F_u = 112 \\ F_w &= 170 \quad w_{Cu} = 9 \quad G = 90 \quad \ddot{w}_{Lu-1} = 1 \\ \alpha \frac{3 + 6 + \ddot{w}_{Pu}}{9 + \ddot{w}_{Pu}} &\leq 112 - 170 - 9 + 90 \\ \alpha \frac{9 + \ddot{w}_{Pu}}{9 + \ddot{w}_{Pu}} &\leq 23 \\ 9 + \ddot{w}_{Pu} &\leq 9 \\ \ddot{w}_{Pu} &\leq \begin{cases} 0 & \text{1ST} \\ 1 & \text{2ND} \end{cases} \end{aligned}$$

STEP 7

WHEN $F_u \leq F_w + w_c u$ THEN

$$\frac{1}{w} \bar{D}_u = 0$$

WHEN $F_u > F_w + w_c u$ THEN

$$\frac{1}{w} \bar{D}_u = \bar{w} L_{u-1} (1 - w_p u)$$

SOLVE FOR $\frac{1}{w} \bar{D}_u$

WHEN $F_u \leq F_w + w_c u$ THE 1ST CAR WILL NOT BE DELAYED AT U. IF THE 1ST CAR IS DELAYED THEN ALL CARS THAT WERE DELAYED AT W AND PASS U-1 WITHOUT DELAY WILL BE DELAYED AT U.

SEE FIGURE 7-1

NOTE:

$$oD_i^- = oD_i$$

$$oD_i^+ = 0 \text{ (EXCEPT FOR IMPRACTICAL CASES)}$$

$$oD_i^{\Delta} = 0$$

NOTE:

WHEN $w_p u > 1$ THEN $\frac{1}{w} \bar{D}_u$ IS NEGATIVE BUT THERE CAN NOT BE A NEGATIVE CAR THEREFORE $\frac{1}{w} \bar{D}_u = 0$.

STEP 8		
WHEN	$dw = 0$ $\frac{\partial}{\partial \bar{w} \bar{u}} = 0$	THEN
WHEN	$dw > 0$ $\frac{\partial}{\partial \bar{w} \bar{u}} = \bar{w} L_{u-1} (1 - w P_u)$	THEN

SOLVE FOR $\frac{\partial}{\partial \bar{w} \bar{u}}$

EXAMPLE:

FIG. 8-1

GIVEN $dw = 7$ $\bar{w} L_{u-1} = 7$ $w P_u = 0$

$\frac{\partial}{\partial \bar{w} \bar{u}} = 7 (1 - 0) = 7$

SEE 2ND NOTE UNDER STEP 7.

STEP 9		
WHEN	$F_u \leq F_w + w P_u$ $\frac{\partial}{\partial \bar{w} \bar{u}} = 0$	THEN
WHEN	$F_u > F_w + w P_u$ $\frac{\partial}{\partial \bar{w} \bar{u}} = \bar{w} L_{u-1} - w P_u$	THEN
	$\bar{w} L_{u-1} = 0$	AND WHEN THEN $\frac{\partial}{\partial \bar{w} \bar{u}} = 0$

SOLVE FOR $\frac{\partial}{\partial \bar{w} \bar{u}}$

EXAMPLE:

FIG. 13-2

GIVEN $\bar{w} L_{u-1} = 4$ $w P_u = 1$ $\frac{\partial}{\partial \bar{w} \bar{u}} = 4 - 1 = 3$

STEP 10

WHEN $dw = 0$ THEN

$$\frac{\partial \Delta}{\partial w} = 0$$

WHEN $dw > 0$ THEN

$$\frac{\partial \Delta}{\partial w} = \bar{w}L_{u-1} - wP_u$$

SOLVE FOR $\frac{\partial \Delta}{\partial w}$

EXAMPLE:

FIG. 13-12

$$\text{GIVEN } dw = 7 \quad \bar{w}L_{u-1} = 7 \quad wP_u = 1 \quad \frac{\partial \Delta}{\partial w} = 7 - 1 = 6$$

STEP 11

$$oP_u^{\hat{}} \leq \frac{N}{C} (F_u - F_i - iC_u) + \frac{1}{2} - wP_u - oL_{\bar{u}-1} - oL_{\bar{u}-1} \quad \text{AND}$$

$$oP_u^{\hat{}} \leq oL_{\bar{u}-1} + oL_{\bar{u}-1} \quad \text{BUT WHEN } oP_{\bar{u}-1}^{\hat{}} = 0$$

$$\text{THEN } oP_u^{\hat{}} = 0$$

SOLVE FOR $oP_u^{\hat{}}$

IN ALL FIGURES

$$F_i - (C-G) - \frac{C}{2N} + \frac{C}{N} (wP_u + oL_{\bar{u}-1} + oL_{\bar{u}-1} + oP_u^{\hat{}}) + iC_u \leq F_u - (C-G)$$

WHICH WHEN TRANSPOSED GIVES THE 1ST PART.

EXAMPLES:

FIG. 11-1

$$\begin{aligned} \text{GIVEN } \frac{N}{C} &= \frac{1}{10} & F_u &= 145 & F_i &= 45 & i_c &= 10 \\ w_{Pu} &= 7 & oL_{\bar{u}-1} &= 0 & oL_{\check{u}-1} &= 1 & oL_{\hat{u}-1} &= 0 \\ oL_{\acute{u}-1} &= 2 \\ oP_{\hat{u}} &\leq \frac{1}{10} (145-45-10) + \frac{1}{2} - 7 - 0 - 1 &&\leq 1 && \leftarrow \text{1ST PART} \\ oP_u &\leq 0 + 2 &&\leq 2 && \text{2ND PART} \end{aligned}$$

FIG. 11-2

$$\begin{aligned} \text{GIVEN } \frac{N}{C} &= \frac{1}{10} & F_u &= 140 & F_i &= 45 & i_c &= 10 \\ w_{Pu} &= 7 & oL_{\bar{u}-1} &= 1 & oL_{\check{u}-1} &= 0 & oL_{\hat{u}-1} &= 1 & oL_{\acute{u}-1} &= 0 \\ oP_{\hat{u}} &\leq \frac{1}{10} (140-45-10) + \frac{1}{2} - 7 - 1 - 0 &&= 1 && \leftarrow \text{1ST PART} \\ oP_u &\leq 1 + 0 &&= 1 && \leftarrow \text{2ND PART} \end{aligned}$$

STEP 12

$$oP\bar{u} \leq \frac{N}{C} (F_u - F_i - iC_u) + \frac{1}{2} - w_{Pu} - 2 oP\hat{u} \quad \text{AND}$$

$$oP\bar{u} \leq oL\bar{u}-1 + oL\hat{u}-1 \quad \text{BUT}$$

$$\text{WHEN} \quad oP\hat{u} = 0 \quad \text{THEN}$$

$$oP\bar{u} = 0$$

SOLVE FOR $oP\bar{u}$

IN ALL FIGURES

$$F_i - (C-G) - \frac{C}{2N} + \frac{C}{N} (w_{Pu} + oP\hat{u} + oP\bar{u}) + iC_u \leq F_u - (C-G) - \frac{C}{N} (oP\hat{u}-1)$$

WHICH WHEN TRANSPOSED GIVES THE 1ST PART.

EXAMPLES:

FIG. 11-1

$$\text{GIVEN } \frac{N}{C} = \frac{1}{10} \quad F_u = 145 \quad F_i = 45 \quad iC_u = 10$$

$$w_{Pu} = 7 \quad oP\hat{u} = 1 \quad oL\bar{u}-1 = 0 \quad oL\hat{u}-1 = 1$$

$$oP\bar{u} \leq \frac{1}{10} (145-45-10) + \frac{1}{2} - 7 - 2 = 1 \quad \leftarrow \text{1ST PART}$$

$$oP\bar{u} \leq 0 + 1 = 1 \quad \leftarrow \text{2ND PART}$$

FIG. 11-2

$$\text{GIVEN } \frac{N}{C} = \frac{1}{10} \quad F_u = 140 \quad F_i = 45 \quad iC_u = 10$$

$$w_{Pu} = 7 \quad oP\hat{u} = 1 \quad oL\bar{u}-1 = 1 \quad oL\hat{u}-1 = 0$$

$$oP\bar{u} \leq \frac{1}{10} (140-45-10) + \frac{1}{2} - 7 - 2 = 1 \quad \leftarrow \text{1ST PART}$$

$$oP\bar{u} \leq 1 + 0 = 1 \quad \leftarrow \text{2ND PART}$$

STEP 13

$$oP_u^{\wedge} \leq \frac{N}{C} (F_u - F_i - i(u)) + \frac{1}{2} - wP_u - \bar{w}D_u^{\wedge} \quad \text{AND}$$

$$oP_u^{\wedge} \leq \left(\begin{array}{l} oL_u^{\wedge} - 1 \quad \text{OR} \\ oL_u^{\wedge} - 1 \end{array} \right) \begin{array}{l} \text{USE} \\ \text{LARGER} \end{array} \quad \text{BUT WHEN } oP_u^{\wedge} > 0$$

$$oP_u^{\wedge} = 0$$

SOLVE FOR oP_u^{\wedge}

IN ALL FIGURES

$$F_i - (C-G) - \frac{C}{2N} + \frac{C}{N} (wP_u + \bar{w}D_u^{\wedge}) + \frac{C}{N} (oP_u^{\wedge}) + i(u) \leq F_u - (C-G)$$

WHICH WHEN TRANSPOSED GIVES THE 1ST PART.

EXAMPLES:

FIG. 13-1

$$\begin{aligned} \text{Given } \frac{N}{C} &= \frac{1}{10} & F_u &= 105 & F_i &= 45 & i(u) &= 10 \\ wP_u &= 4 & \bar{w}D_u^{\wedge} &= 0 & oL_u^{\wedge} - 1 &= 0 & oL_u^{\wedge} - 1 &= 6 & oP_u^{\wedge} &= 0 \\ oP_u^{\wedge} &\leq \frac{1}{10} (105 - 45 - 10) + \frac{1}{2} - 4 - 0 & &= & 1 & + & \text{1ST} \\ oP_u^{\wedge} &\leq 0 \text{ OR } 6 & &= & 6 & & \text{2ND} \end{aligned}$$

FIG. 13-2

$$\begin{aligned} \text{GIVEN } \frac{N}{C} &= \frac{1}{10} & F_u &= 80 & F_i &= 45 & i(u) &= 5 \\ wP_u &= 1 & \bar{w}D_u^{\wedge} &= 3 & oL_u^{\wedge} - 1 &= 0 & oL_u^{\wedge} - 1 &= 6 & oP_u^{\wedge} &= 0 \\ oP_u^{\wedge} &\leq \frac{1}{10} (80 - 45 - 5) + \frac{1}{2} - 1 - 3 & &= & 0 & + & \text{1ST} \\ oP_u^{\wedge} &\leq 0 \text{ OR } 6 & &= & 6 & & \text{2ND} \end{aligned}$$

FIG. 13-3

$$\begin{aligned} \text{GIVEN } \frac{N}{C} &= \frac{1}{10} & F_u &= 135 & F_i &= 45 & i(u) &= 10 \\ wP_u &= 6 & \bar{w}D_u^{\wedge} &= 0 & oL_u^{\wedge} - 1 &= 0 & oL_u^{\wedge} - 1 &= 4 & oP_u^{\wedge} &= 0 \\ oP_u^{\wedge} &\leq \frac{1}{10} (135 - 45 - 10) + \frac{1}{2} - 6 - 0 & &= & 2 & + & \text{1ST} \\ oP_u^{\wedge} &\leq 0 \text{ OR } 4 & &= & 4 & & \text{2ND} \end{aligned}$$

FIG. 13-4

$$\begin{aligned} \text{GIVEN } \frac{N}{C} &= \frac{1}{10} & F_u &= 145 & F_i &= 45 & iC_u &= 10 \\ w_{Pu} &= 7 & \bar{w}_{Du}^{\Delta} &= 0 & oL_{u-i}^{\leftarrow} &= 0 & oL_{u-i}^{\rightarrow} &= 3 & oP_u^{\Delta} &= 0 \\ oP_u^{\leftarrow} &\leq \frac{1}{10} (145-45-10) + \frac{1}{2} - 7 - 0 & & & & & & & &= 2 \leftarrow \text{1ST} \\ oP_u^{\rightarrow} &\leq 0 \text{ OR } 3 & & & & & & & &= 3 \quad \text{2ND} \end{aligned}$$

FIG. 13-5

$$\begin{aligned} \text{GIVEN } \frac{N}{C} &= \frac{1}{10} & F_u &= 135 & F_i &= 45 & iC_u &= 10 \\ w_{Pu} &= 7 & \bar{w}_{Du}^{\Delta} &= 0 & oL_{u-i}^{\leftarrow} &= 0 & oL_{u-i}^{\rightarrow} &= 3 & oP_u^{\Delta} &= 0 \\ oP_u^{\leftarrow} &\leq \frac{1}{10} (135-45-10) + \frac{1}{2} - 7 - 0 & & & & & & & &= 1 \leftarrow \text{1ST} \\ oP_u^{\rightarrow} &\leq 0 \text{ OR } 3 & & & & & & & &= 3 \quad \text{2ND} \end{aligned}$$

FIG. 13-6

$$\begin{aligned} \text{GIVEN } \frac{N}{C} &= \frac{1}{10} & F_u &= 160 & F_i &= 45 & iC_u &= 9 \\ w_{Pu} &= 4 & \bar{w}_{Du}^{\Delta} &= 0 & oL_{u-i}^{\leftarrow} &= 4 & oL_{u-i}^{\rightarrow} &= 0 & oP_u^{\Delta} &= 0 \\ oP_u^{\leftarrow} &\leq \frac{1}{10} (160-45-9) + \frac{1}{2} - 4 - 0 & & & & & & & &= 7 \quad \text{1ST} \\ oP_u^{\rightarrow} &\leq 4 \text{ OR } 0 & & & & & & & &= 4 \leftarrow \text{2ND} \end{aligned}$$

FIG. 13-7

$$\begin{aligned} \text{GIVEN } \frac{N}{C} &= \frac{1}{10} & F_u &= 180 & F_i &= 35 & iC_u &= 11 \\ w_{Pu} &= 6 & \bar{w}_{Du}^{\Delta} &= 0 & oL_{u-i}^{\leftarrow} &= 3 & oL_{u-i}^{\rightarrow} &= 0 & oP_u^{\Delta} &= 0 \\ oP_u^{\leftarrow} &\leq \frac{1}{10} (180-35-11) + \frac{1}{2} - 6 - 0 & & & & & & & &= 7 \quad \text{1ST} \\ oP_u^{\rightarrow} &\leq 3 \text{ OR } 0 & & & & & & & &= 3 \leftarrow \text{2ND} \end{aligned}$$

FIG. 13-8

$$\begin{aligned} \text{GIVEN } \frac{N}{C} &= \frac{1}{10} & F_u &= 180 & F_i &= 35 & iC_u &= 12 \\ w_{Pu} &= 7 & \bar{w}_{Du}^{\Delta} &= 0 & oL_{u-i}^{\leftarrow} &= 2 & oL_{u-i}^{\rightarrow} &= 0 & oP_u^{\Delta} &= 0 \\ oP_u^{\leftarrow} &\leq \frac{1}{10} (180-35-12) + \frac{1}{2} - 7 - 0 & & & & & & & &= 6 \quad \text{1ST} \\ oP_u^{\rightarrow} &\leq 2 \text{ OR } 0 & & & & & & & &= 2 \leftarrow \text{2ND} \end{aligned}$$

FIG. 13-9

$$\begin{aligned} \text{GIVEN } \frac{N}{C} &= \frac{1}{10} & F_u &= 105 & F_l &= 45 & i(\bar{C}_u) &= 10 \\ w_{Pu} &= 4 & \bar{w}_{D_u} &= 0 & oL_{u-1} &= 4 & oL'_{u-1} &= 0 & oP_u^{\wedge} &= 0 \\ oP_u^{\leftarrow} &\leq \frac{1}{10} (105-45-10) + \frac{1}{2} - 4 - 0 & & & & & & & &= 1 \leftarrow \text{1ST} \\ oP_u^{\leftarrow} &\leq 4 \text{ OR } 0 & & & & & & & &= 4 \quad \text{2ND} \end{aligned}$$

FIG. 13-10

$$\begin{aligned} \text{GIVEN } \frac{N}{C} &= \frac{1}{10} & F_u &= 145 & F_l &= 45 & i(\bar{C}_u) &= 10 \\ w_{Pu} &= 7 & \bar{w}_{D_u} &= 0 & oL_{u-1} &= 1 & oL'_{u-1} &= 1 & oP_u^{\wedge} &= 0 \\ oP_u^{\leftarrow} &\leq \frac{1}{10} (145-45-10) + \frac{1}{2} - 7 - 0 & & & & & & & &= 2 \quad \text{1ST} \\ oP_u^{\leftarrow} &\leq 1 \text{ OR } 1 & & & & & & & &= 1 \leftarrow \text{2ND} \end{aligned}$$

FIG. 13-11

$$\begin{aligned} \text{GIVEN } \frac{N}{C} &= \frac{1}{10} & F_u &= 175 & F_l &= 30 & i(\bar{C}_u) &= 13 \\ w_{Pu} &= 7 & \bar{w}_{D_u} &= 0 & oL_{u-1} &= 1 & oL'_{u-1} &= 0 & oP_u^{\wedge} &= 0 \\ oP_u^{\leftarrow} &\leq \frac{1}{10} (175-30-13) + \frac{1}{2} - 7 - 0 & & & & & & & &= 6 \quad \text{1ST} \\ oP_u^{\leftarrow} &\leq 1 \text{ OR } 0 & & & & & & & &= 1 \leftarrow \text{2ND} \end{aligned}$$

FIG. 13-12

$$\begin{aligned} \text{GIVEN } \frac{N}{C} &= \frac{1}{10} & F_u &= 100 & F_l &= 30 & i(\bar{C}_u) &= 13 \\ w_{Pu} &= 1 & \bar{w}_{D_u} &= 6 & oL_{u-1} &= 4 & oL'_{u-1} &= 0 & oP_u^{\wedge} &= 0 \\ oP_u^{\leftarrow} &\leq \frac{1}{10} (100-30-13) + \frac{1}{2} - 1 - 6 = -1 & & & & & & & &= 0 \leftarrow \text{1ST} \\ oP_u^{\leftarrow} &\leq 4 \text{ OR } 0 & & & & & & & &= 4 \quad \text{2ND} \end{aligned}$$

STEP 14

$$a_u = w_{Pu} + o_{Pu}$$

SOLVE FOR a_u

FIGURE 11-2 ILLUSTRATES a_u .

EXAMPLE:

FIG. 11-2

$$\text{GIVEN } w_{Pu} = 7 \quad o_{Pu} = 2$$

$$a_u = 7 + 2 = 9$$

STEP 15

$$q \frac{w_{Dv} + w_{dv} + w_{D\bar{u}}}{w_{D\bar{u}}} - q \frac{a_w - a_u + w_{Dv} + w_{dv} + w_{D\bar{u}}}{w_{D\bar{u}}} < F_u - F_w - w_{Cu}$$

AND $w_{D\bar{u}} \leq w_{Lu-1}$ BUT WHEN $a_u \geq a_w$ THEN $w_{D\bar{u}} = 0$ AND WHEN

$$F_w + q \frac{w_{Dv} + w_{dv} + 1}{w_{D\bar{u}}} + w_{Cu} \geq F_u + q \frac{a_w - a_u + w_{Dv} + w_{dv} + 1}{w_{D\bar{u}}} \text{ THEN } w_{D\bar{u}} = 0$$

SOLVE FOR $w_{D\bar{u}}$

IN ALL FIGURES

$$F_w + q \frac{w_{Dv} + w_{dv} + w_{D\bar{u}}}{w_{D\bar{u}}} + w_{Cu} < F_u + q \frac{a_w - a_u + w_{Dv} + w_{dv} + w_{D\bar{u}}}{w_{D\bar{u}}}$$

WHICH WHEN TRANSPOSED GIVES THE FIRST PART OF STEP 15

EXAMPLES:

$$\text{FIG. 15-1} \quad \text{GIVEN } w_{Dv} = 0 \quad w_{dv} = 0 \quad a_w = 7 \quad a_u = 2 \quad F_u = 101$$

$$F_w = 100 \quad w_{Cu} = 11 \quad w_{Lu-1} = 3$$

$$q \frac{0+0+w_{D\bar{u}}}{w_{D\bar{u}}} - q \frac{7-2+0+0+w_{D\bar{u}}}{w_{D\bar{u}}} < 101 - 100 - 11$$

$$q \frac{w_{D\bar{u}}}{w_{D\bar{u}}} - q \frac{5+w_{D\bar{u}}}{w_{D\bar{u}}} < -10$$

$$w_{D\bar{u}} = 1 \quad \leftarrow \text{1ST PART}$$

$$w_{D\bar{u}} \leq 3 \quad \text{2ND PART}$$

FIG. 15-2 GIVEN $\acute{w}D\bar{v} = 0$ $\acute{w}dv = 0$ $a_w = 7$ $a_u = 3$ $F_u = 120$

$$F_w = 100 \quad w\bar{c}_u = 11 \quad \acute{w}L_{u-1} = 4$$

$$d \frac{0+0+\acute{w}D\bar{u}}{\acute{w}D\bar{u}} - d \frac{7-3+0+0+\acute{w}D\bar{u}+1}{5+\acute{w}D\bar{u}} < 120 - 100 - 11$$

$$d \frac{\acute{w}D\bar{u}}{\acute{w}D\bar{u}} - d \frac{5+\acute{w}D\bar{u}}{\acute{w}D\bar{u}} < 9$$

$$\acute{w}D\bar{u} = \infty \quad \text{1ST PART}$$

$$\acute{w}D\bar{u} = 4 \quad \leftarrow \quad \text{2ND PART}$$

FIG. 15-3 GIVEN $\acute{w}D\bar{v} = 1$ $\acute{w}dv = 0$ $a_w = 7$ $a_u = 3$ $F_u = 125$

$$F_w = 118 \quad w\bar{c}_u = 10 \quad \acute{w}L_{u-1} = 4$$

$$d \frac{1+0+\acute{w}D\bar{u}}{1+\acute{w}D\bar{u}} - d \frac{7-3+1+0+\acute{w}D\bar{u}+1}{6+\acute{w}D\bar{u}} < 125 - 118 - 10$$

$$d \frac{1+\acute{w}D\bar{u}}{1+\acute{w}D\bar{u}} - d \frac{6+\acute{w}D\bar{u}}{6+\acute{w}D\bar{u}} < -3$$

$$\acute{w}D\bar{u} = \infty \quad \text{1ST PART}$$

$$\acute{w}D\bar{u} = 4 \quad \leftarrow \quad \text{2ND PART}$$

FIG. 15-4 GIVEN $\acute{w}D\bar{v} = 0$ $\acute{w}dv = 1$ $a_w = 7$ $a_u = 4$ $F_u = 140$

$$F_w = 100 \quad w\bar{c}_u = 11 \quad \acute{w}L_{u-1} = 3$$

$$d \frac{1+\acute{w}D\bar{u}}{1+\acute{w}D\bar{u}} - d \frac{4+\acute{w}D\bar{u}+1}{4+\acute{w}D\bar{u}+1} < 29$$

$$\acute{w}D\bar{u} = \infty \quad \text{1ST PART}$$

$$\acute{w}D\bar{u} = 3 \quad \leftarrow \quad \text{2ND PART}$$

STEP 16

WHEN $F_u \leq F_w + w\bar{C}_u$ THEN

$$\dot{w}D\bar{u}^{\square} = 0$$

WHEN $F_u > F_w + w\bar{C}_u$ THEN

$$\dot{w}D\bar{u}^{\square} = \dot{w}L_{u-1} - \dot{w}P_u - \dot{w}D\bar{u}$$

SOLVE FOR $\dot{w}D\bar{u}^{\square}$

THE $\dot{w}D\bar{u}^{\square}$ IS ILLUSTRATED IN FIG. 16-1 BY $\dot{3}D\bar{4}$ AND SINCE $\dot{w}D\bar{u}^{\square}$ INCLUDES $\dot{w}D\bar{u}$ AND $\dot{w}D\bar{u}^{\Delta}$ THEN $\dot{w}D\bar{u}^{\square}$ IS ALSO ILLUSTRATED BY $\dot{1}D\bar{2}$, $\dot{2}D\bar{5}$, $\dot{5}D\bar{6}$, $\dot{6}D\bar{7}$ AND $\dot{2}D\bar{3}$.

SEE ALSO FIG. 13-12: $\dot{3}D\bar{u}^{\square} = 6$

STEP 17

$$\frac{C}{N}(\dot{o}D\bar{u}^{\vec{3}}) - \alpha \frac{\bar{w}D\bar{u}^{\Delta} + \dot{o}D\bar{u}^{\vec{3}}}{\dot{o}D\bar{u}^{\vec{3}}} < F_u - F_l - i\bar{C}_u + \frac{C}{2N} + (C-G) - \frac{C}{N}(\dot{a}_u + \bar{w}D\bar{u}^{\Delta})$$

$$\dot{o}D\bar{u}^{\vec{3}} \leq \dot{o}L_{\bar{u}-1} - \dot{o}P_{\bar{u}}$$

SOLVE FOR $\dot{o}D\bar{u}^{\vec{3}}$

IN ALL FIGURES

$$F_l - (C-G) - \frac{C}{2N} + \frac{C}{N}(\dot{a}_u + \bar{w}D\bar{u}^{\Delta}) + \frac{C}{N}(\dot{o}D\bar{u}^{\vec{3}}) + i\bar{C}_u <$$

$$F_u + \alpha \frac{\bar{w}D\bar{u}^{\Delta} + \dot{o}D\bar{u}^{\vec{3}}}{\dot{o}D\bar{u}^{\vec{3}}}$$

WHICH WHEN TRANSPOSED EQUALS THE FIRST PART OF STEP 17.

EXAMPLES:

FIG. 17-1 GIVEN $\bar{w}\hat{D}\hat{u} = 3$ $F_u = 85$ $F_l = 45$ $i\hat{C}_u = 10$ $\frac{C}{N} = 10$
 $(C-G) = 25$ $a_u = 1$ $oL\hat{u}-1 = 1$ $oP\hat{u} = 0$
 $10 (oD\hat{u}) - \alpha' \frac{3+oD\hat{u}}{2} < 85 - 45 - 10 + 5 + 25 - 10 (1+3)$
 $10 (oD\hat{u}) - \alpha' \frac{3+oD\hat{u}}{2} < 20$
 $oD\hat{u} = 3$ } 1ST PART
 $oD\hat{u} \leq 1-0 = 1$ } + 2ND PART

STEP 18

$$\frac{C}{N} (oD\hat{u}) - \alpha' \frac{wD_u + oD\hat{u}}{2} < F_u - F_l - i\hat{C}_u + \frac{C}{2N} + (C-G) - \frac{C}{N} (a_u - 1 - oL\hat{u} - 1)$$

$$oD\hat{u} \leq oL\hat{u} - 1 - oP\hat{u}$$

SOLVE FOR $oD\hat{u}$

IN ALL FIGURES

$$F_l - (C-G) - \frac{C}{2N} + \frac{C}{N} (a_u - 1 - oL\hat{u} - 1) + \frac{C}{N} (oD\hat{u}) + i\hat{C}_u <$$

$$F_u + \alpha' \frac{wD_u + oD\hat{u}}{2}$$

WHICH WHEN TRANSPOSED GIVES THE 1ST PART.

EXAMPLE:

FIG. 18-1 GIVEN $\frac{C}{N} = 10$ $wD_u = 3$ $F_u = 120$ $F_l = 45$ $i\hat{C}_u = 10$
 $(C-G) = 25$ $a_u - 1 = 9$ $oL\hat{u} - 1 = 1$ $oP\hat{u} = 0$
 $10 (oD\hat{u}) - \alpha' \frac{3+oD\hat{u}}{2} < 120 - 45 - 10 + 5 + 25 - 10 (9-1)$
 $10 (oD\hat{u}) - \alpha' \frac{3+oD\hat{u}}{2} < 15$
 $oD\hat{u} = \left\{ \begin{array}{l} 3 \quad 1ST \ PART \\ 1-0 = 1 \quad + \quad 2ND \ PART \end{array} \right.$

STEP 19

$$\frac{C}{N} (oD\acute{u}) - \alpha \frac{\bar{w}D\acute{u} + oD\acute{u}}{1} < F_u - F_l - iC_u + \frac{C}{2N} + (C-G) - \frac{C}{N} (a_u + \bar{w}D\acute{u})$$

$$oD\acute{u} \leq oL\acute{u}-1 - oP\acute{u}$$

SOLVE FOR $oD\acute{u}$

IN ALL FIGURES

$$F_l - (C-G) - \frac{C}{2N} + \frac{C}{N} (a_u + \bar{w}D\acute{u}) + \frac{C}{N} (oD\acute{u}) + iC_u <$$

$$F_u + \alpha \frac{\bar{w}D\acute{u} + oD\acute{u}}{1}$$

WHICH WHEN TRANSPOSED GIVES PART 1.

EXAMPLES:

FIG. 19-1 GIVEN $\frac{C}{N} = 10$ $\bar{w}D\acute{u} = 1$ $F_u = 90$ $F_l = 45$ $iC_u = 10$

$(C-G) = 25$ $a_u = 3$ $oL\acute{u}-1 = 3$ $oP\acute{u} = 0$

$$10 (oD\acute{u}) - \alpha \frac{1+oD\acute{u}}{1} < 90 - 45 - 10 + 5 + 25 - 10 (3+1)$$

$$10 (oD\acute{u}) - \alpha \frac{1+oD\acute{u}}{1} < 25$$

$$oD\acute{u} = \begin{cases} 3 & \leftarrow \text{PART 1} \\ 3-0 = 3 & \leftarrow \text{PART 2} \end{cases}$$

FIG. 19-2 GIVEN $\frac{C}{N} = 10$ $\bar{w}D\acute{u} = 0$ $F_u = 125$ $F_l = 35$ $iC_u = 10$

$(C-G) = 25$ $a_u = 8$ $oL\acute{u}-1 = 3$ $oP\acute{u} = 2$

$$10 (oD\acute{u}) - \alpha \frac{0+oD\acute{u}}{1} < 125 - 35 - 10 + 5 + 25 - 10 (8-0)$$

$$10 (oD\acute{u}) - \alpha \frac{oD\acute{u}}{1} < 30$$

$$oD\acute{u} = \begin{cases} \infty & \leftarrow \text{1ST PART} \\ 3-2 = 1 & \leftarrow \text{2ND PART} \end{cases}$$

STEP 20

$$\frac{C}{N} (oDú) - q \frac{wD\bar{u} + wD\bar{u} + oDú}{N} \quad F_u - F_i - iC_u + \frac{C}{2N} + (C-G) - \frac{C}{N} (Q_u + wD\bar{u} + wD\bar{u})$$

$$oDú \leq N - Q_u - wD_u \quad \text{BUT WHEN } oL_u - i = 0$$

$$\text{THEN } oDú = 0$$

SOLVE FOR $oDú$

IN ALL FIGURES

$$F_i - (C-G) - \frac{C}{2N} + \frac{C}{N} (Q_u + wD\bar{u} + wD\bar{u}) + \frac{C}{N} (oDú) + iC_u <$$

$$F_u + q \frac{wD\bar{u} + wD\bar{u} + oDú}{N}$$

WHICH WHEN TRANSPOSED EQUALS THE FIRST PART OF STEP 20.

EXAMPLES:

FIG. 13-4 GIVEN $wD\bar{u} = 0$ $wD\bar{u} = 0$ $F_u = 145$ $F_i = 45$ $iC_u = 10$

$$\frac{C}{N} = 10 \quad (C-G) = 25 \quad Q_u = 9 \quad N = 10 \quad wD_u = 0$$

$$10 (oDú) - q \frac{0+0+oDú}{10} < 145 - 45 - 10 + 5 + 25 - 10 (9+0+0)$$

$$10 (oDú) - q \frac{oDú}{10} < 30$$

$$oDú = \begin{cases} 4 & \text{1ST PART} \\ (10-9) = 1 & \text{2ND PART} \end{cases}$$

FIG. 20-1 GIVEN $wD\bar{u} = 1$ $wD\bar{u} = 4$ $F_u = 125$ $F_i = 50$ $iC_u = 11$

$$\frac{C}{N} = 10 \quad (C-G) = 30 \quad Q_u = 5 \quad N = 12 \quad wD_u = 5$$

$$10 (oDú) - q \frac{1+4+oDú}{12} < 125 - 50 - 11 + 5 + 30 - 10 (5+1+4)$$

$$10 (oDú) - q \frac{5+oDú}{12} < -1$$

$$oDú = \begin{cases} 1 & \text{1ST PART} \\ (12 - 5 - 5) = 2 & \text{2ND PART} \end{cases}$$

STEP 21

$$Du = wD\bar{u} + \frac{1}{w}D\hat{u} + wD\bar{u} + oD\bar{u} + oD\hat{u} + oD\bar{u} + oD\hat{u}$$

SOLVE FOR Du

STEP 22

$$Hu = \left(\begin{array}{c} \alpha \frac{Du}{u} \\ Hu-1 - Fu + Fu-1 + u-1\bar{u} \end{array} \right) \text{ OR } \left(\begin{array}{c} \alpha \frac{Du}{u} \\ Hu-1 - Fu + Fu-1 + u-1\hat{u} \end{array} \right) \text{ USE LARGER}$$

SOLVE FOR Hu

IN FIG. 22-1

$$Hu = \alpha \frac{Du}{u} \text{ WHICH IS LARGER THAN } Hu-1 - Fu + Fu-1 + u-1\bar{u}$$

IN FIG. 22-2

$$Hu = Hu-1 - Fu + Fu-1 + u-1\hat{u} \text{ WHICH IS LARGER THAN } \alpha \frac{Du}{u}$$

THESE TWO FIGURES ILLUSTRATE THE POSSIBLE VARIATIONS OF Hu.

STEP 23

$$\begin{aligned}
 & \alpha \frac{\dot{w}_{du}}{\dot{w}_{du}} - \alpha \frac{D_u + a_w + \dot{w}_{du}}{\dot{w}_{du}} < F_u - F_w - w_c u - C \quad \text{AND} \\
 & \dot{w}_{du} \leq \dot{w}_{pu} \\
 & F_w + \alpha \frac{1}{\dot{w}_{du}} + w_c u \Rightarrow F_u - C + \alpha \frac{D_u + a_w + 1}{\dot{w}_{du}} \quad \text{BUT WHEN THEN} \\
 & \dot{w}_{du} = 0
 \end{aligned}$$

SOLVE FOR \dot{w}_{du}

IN FIGURES 23-1 AND 23-2

$$\begin{aligned}
 & F_w + \alpha \frac{\dot{w}_{du}}{\dot{w}_{du}} + w_c u < F_u - C + \alpha \frac{D_u + a_w + \dot{w}_{du}}{\dot{w}_{du}} \\
 & \text{WHICH WHEN TRANSPOSED GIVES THE 1ST PART.}
 \end{aligned}$$

EXAMPLES:

FIG. 23-1 GIVEN $D_u = 1$ $a_w = 3$ $F_u = 188$ $F_w = 65$ $w_c u = 11$

$$C = 120 \quad \dot{w}_{pu} = 3$$

$$\alpha \frac{\dot{w}_{du}}{\dot{w}_{du}} - \alpha \frac{1+3+\dot{w}_{du}}{\dot{w}_{du}} < 188 - 65 - 11 - 120$$

$$\alpha \frac{\dot{w}_{du}}{\dot{w}_{du}} - \alpha \frac{4+\dot{w}_{du}}{\dot{w}_{du}} < -8$$

$$\dot{w}_{du} = \begin{cases} 1 & \text{1ST PART} \\ 3 & \text{2ND PART} \end{cases}$$

FIG. 23-2 GIVEN $D_u = 1$ $a_w = 0$ $F_u = 190$ $F_w = 60$ $w_c u = 6$

$$C = 100 \quad \dot{w}_{pu} = 6$$

$$\alpha \frac{\dot{w}_{du}}{\dot{w}_{du}} - \alpha \frac{1+0+\dot{w}_{du}}{\dot{w}_{du}} < 190 - 60 - 6 - 100$$

$$\alpha \frac{\dot{w}_{du}}{\dot{w}_{du}} - \alpha \frac{1+\dot{w}_{du}}{\dot{w}_{du}} < 24$$

$$\dot{w}_{du} = \begin{cases} \infty & \text{1ST PART} \\ 6 & \text{2ND PART} \end{cases}$$

STEP 24

$$\begin{aligned}
 & \alpha \frac{Dw + \ddot{w}_{du}}{\ddot{w}_{du} \leq \ddot{w}_{Pu}} - \alpha \frac{Du + \ddot{w}_{du}}{dw = 0} < Fu - Fw - wCu \quad \text{AND WHEN} \\
 & \text{WHEN } \alpha \frac{Du}{Dw} - \alpha \frac{Dw}{Dw} \leq Fw - Fu + wCu \quad \text{THEN } \ddot{w}_{du} = 0
 \end{aligned}$$

SOLVE FOR \ddot{w}_{du}

IN FIGURES 24-1 AND 24-2

$$Fw - C + \alpha \frac{Dw + \ddot{w}_{du}}{\ddot{w}_{du}} + wCu < Fu - C + \alpha \frac{Du + \ddot{w}_{du}}{\ddot{w}_{du}}$$

WHICH WHEN TRANSPOSED GIVES THE 1ST PART.

EXAMPLES:

FIG. 24-1 GIVEN $Dw = 3$ $Du = 5$ $Fu = 174$

$$Fw = 170 \quad wCu = 7.5 \quad \ddot{w}_{Pu} = 7$$

$$\alpha \frac{3 + \ddot{w}_{du}}{\ddot{w}_{du}} - \alpha \frac{5 + \ddot{w}_{du}}{\ddot{w}_{du}} < 174 - 170 - 7.5$$

$$\alpha \frac{3 + \ddot{w}_{du}}{\ddot{w}_{du}} - \alpha \frac{5 + \ddot{w}_{du}}{\ddot{w}_{du}} < -3.5$$

$$\ddot{w}_{du} = \begin{cases} 6 & \leftarrow \text{1ST PART} \\ 7 & \leftarrow \text{2ND PART} \end{cases}$$

FIG. 24-2 GIVEN $Dw = 1$ $Du = 1$ $Fu = 190$

$$Fw = 175 \quad wCu = 7 \quad \ddot{w}_{Pu} = 7$$

$$\alpha \frac{1 + \ddot{w}_{du}}{\ddot{w}_{du}} - \alpha \frac{1 + \ddot{w}_{du}}{\ddot{w}_{du}} < 190 - 175 - 7$$

$$\alpha \frac{1 + \ddot{w}_{du}}{\ddot{w}_{du}} - \alpha \frac{1 + \ddot{w}_{du}}{\ddot{w}_{du}} < 8$$

$$\ddot{w}_{du} = \begin{cases} \infty & \leftarrow \text{1ST PART} \\ 7 & \leftarrow \text{2ND PART} \end{cases}$$

STEP 25

$$\frac{C}{N} (\text{odu}) - \alpha' \frac{Du + \hat{w}du + \text{odu}}{\quad} < Fu - F_1 - iC_u + \frac{C}{2N} - G - \frac{C}{N} (\hat{w}du)$$

$$\text{odu} \leq \text{oP}\hat{u} + \text{oP}\hat{u}$$

SOLVE FOR odu

IN FIGURES 25-1 AND 25-2

$$F_1 - (C-G) - \frac{C}{2N} + \frac{C}{N} (\hat{w}du) + \frac{C}{N} (\text{odu}) + iC_u < Fu - C + \alpha' \frac{Du + \hat{w}du + \text{odu}}{\quad}$$

WHICH WHEN TRANSPOSED GIVES THE 1ST PART.

EXAMPLES:

FIG. 25-1 GIVEN $\frac{C}{N} = 10$ $Du = 1$ $\hat{w}du = 6$ $Fu = 180$

$F_1 = 35$ $iC_u = 11$ $G = 75$ $\text{oP}\hat{u} = 0$ $\text{oP}\hat{u} = 3$

$$10 (\text{odu}) - \alpha' \frac{1+6+\text{odu}}{\quad} < 180 - 35 - 11 + 5 - 75 - 10 (6)$$

$$10 (\text{odu}) - \alpha' \frac{7+\text{odu}}{\quad} < 4$$

$$\text{odu} = \begin{cases} 2 & \leftarrow \text{1ST PART} \\ 3 & \leftarrow \text{2ND PART} \end{cases}$$

FIG. 25-2 GIVEN $\frac{C}{N} = 10$ $Du = 1$ $\hat{w}du = 4$ $Fu = 190$

$F_1 = 45$ $iC_u = 11.5$ $G = 75$ $\text{oP}\hat{u} = 1$ $\text{oP}\hat{u} = 0$

$$10 (\text{odu}) - \alpha' \frac{1+4+\text{odu}}{\quad} < 190 - 45 - 11.5 + 5 - 75 - 10 (4)$$

$$10 (\text{odu}) - \alpha' \frac{5+\text{odu}}{\quad} < 23.5$$

$$\text{odu} = \begin{cases} 4 & \leftarrow \text{1ST PART} \\ 1 & \leftarrow \text{2ND PART} \end{cases}$$

NOTE: THERE CANNOT BE AN \hat{u} .

STEP 26

$$\acute{w}L\acute{u}'' = \acute{w}P_u - \acute{w}d_u$$

SOLVE FOR $\acute{w}L\acute{u}''$

EXAMPLES:

FIG. 23-1 GIVEN $\acute{w}P_u = 3$ $\acute{w}d_u = 1$

$$\acute{w}L\acute{u}'' = 3 - 1 = 2$$

STEP 27

$$wL\acute{u}'' = wP_u - w\acute{d}_u$$

SOLVE FOR $wL\acute{u}''$

EXAMPLES:

FIG. 24-1 GIVEN $wP_u = 7$ $w\acute{d}_u = 6$

$$wL\acute{u}'' = 7 - 6 = 1$$

STEP 28

$$\acute{w}L\acute{u}' = \acute{w}L_{u-1} - \acute{w}D_u - \acute{w}P_u$$

SOLVE FOR $\acute{w}L\acute{u}'$

EXAMPLES:

FIG. 15-1 GIVEN $\acute{w}L_{u-1} = 3$ $\acute{w}D_u = 1$ $\acute{w}P_u = 0$

$$\acute{w}L\acute{u}' = 3 - 1 - 0 = 2$$

FIG. 5-1 GIVEN $\bar{w}Lu-1 = 5$ $\bar{w}Du = 1$ $\bar{w}Pu = 4$
 $\bar{w}Lu = 5 - 1 - 4 = 0$

NOTE: $\bar{w}Lu = 0$ A CONDITION WHICH WOULD GIVE A POSITIVE VALUE
 FOR $\bar{w}Lu$ CANNOT EXIST.

STEP 29

$D\bar{u} = \bar{w}D\bar{u} + \bar{w}D\bar{u} + oD\bar{u} + oD\bar{u}$ BUT
 WHEN $\bar{w}D\bar{u} = 0$ THEN
 $D\bar{u} = 0$

SOLVE FOR $D\bar{u}$

EXAMPLES:

FIG. 8-1 GIVEN $\bar{w}D\bar{u} = 7$ $\bar{w}D\bar{u} = 0$ $oD\bar{u} = 0$ $oD\bar{u} = 4$
 $D\bar{u} = 7 + 0 + 0 + 4 = 11$

FIG. 7-1 GIVEN $\bar{w}D\bar{u} = 6$ $\bar{w}D\bar{u} = 0$ $oD\bar{u} = 0$ $oD\bar{u} = 2$
 $D\bar{u} = 6 + 0 + 0 + 2 = 8$

FIG. 13-1 GIVEN $\bar{w}D\bar{u} = 0$ $\bar{w}D\bar{u} = 0$ $oD\bar{u} = 0$ $oD\bar{u} = 0$
 SINCE $Du = 0$ THEN $Du = 0$

SINCE THE GROUP OF CARS FROM w TO u INCLUDING THE
 1ST CAR IS NOT DELAYED THE D CARS AT u DO NOT INCLUDE
 THE FIRST CAR.

STEP 30

$$\bar{w}Lu = \bar{w}Lu-1 - wDu + \acute{w}D\bar{u} \quad \text{BUT WHEN } wdu > 0$$

$$\text{THEN } \bar{w}Lu = 0 \quad \text{AND}$$

$$\text{WHEN } \bar{w}Lu-1 = 0 \quad \text{THEN } \bar{w}Lu = 0$$

SOLVE FOR $\bar{w}Lu$

EXAMPLES:

FIG. 13-2 GIVEN $\bar{w}Lu-1 = 4$ $wDu = 3$ $\acute{w}D\bar{u} = 0$ $wdu = 0$

$$\bar{w}Lu = 4 - 3 + 0 = 1$$

FIG. 13-12 GIVEN $\bar{w}Lu-1 = 7$ $wDu = 6$ $\acute{w}D\bar{u} = 0$ $wdu = 0$

$$\bar{w}Lu = 7 - 6 + 0 = 1$$

FIG. 5-1 GIVEN $\bar{w}Lu-1 = 5$ $wDu = 1$ $\acute{w}D\bar{u} = 0$ $wdu = 0$

$$\bar{w}Lu = 5 - 1 + 0 = 4$$

FIG. 5-5 GIVEN $\bar{w}Lu-1 = 7$ $wDu = 0$ $\acute{w}D\bar{u} = 0$ $wdu = 1$

$$\bar{w}Lu = 0$$

STEP 31

$$oL\bar{u} = oP\bar{u} - odu$$

SOLVE FOR $oL\bar{u}$

EXAMPLES:

FIG. 11-1 GIVEN $oP\bar{u} = 1$ $odu = 0$ $oL\bar{u} = 1 - 0 = 1$

FIG. 11-2 GIVEN $oP\bar{u} = 1$ $odu = 0$ $oL\bar{u} = 1 - 0 = 1$

STEP 32

$$oL\hat{u} = oP\hat{u}$$

SOLVE FOR $oL\hat{u}$

EXAMPLE:

FIG. 11-1 GIVEN $oP\hat{u} = 1$

$$oL\hat{u} = 1$$

STEP 33

$$oL\acute{u} = N - a_u - D_u - vL\acute{u}$$

SOLVE FOR $oL\acute{u}$

EXAMPLE:

FIG. 20-1 GIVEN $N = 12$ $a_u = 5$ $D_u = 6$ $vL\acute{u} = 0$

$$oL\acute{u} = 12 - 5 - 6 - 0 = 1$$

FIG. 17-1 GIVEN $N = 10$ $a_u = 1$ $D_u = 4$ $vL\acute{u} = 4$

$$oL\acute{u} = 10 - 1 - 4 - 4 = 1$$

STEP 33A

$$oL\acute{u} = oP\acute{u} - odu$$

SOLVE FOR $oL\acute{u}$

EXAMPLE:

FIG. 13-7 GIVEN $oP\acute{u} = 3$ $odu = 2$

$$oL\acute{u} = 3 - 2 = 1$$

STEP 34

$$\bar{o}L\acute{x} = oL\acute{x}-1 + oL\bar{x}-1 - oDx - oL\bar{x} - oDx + oD\acute{x}$$

SOLVE FOR $\bar{o}L\acute{x}$

EXAMPLE:

FIG. 13-6 GIVEN $oL\acute{x}-1 = 4$ $oL\bar{x}-1 = 0$ $oDx = 1$ $oL\bar{x} = 0$ $oDx = 0$ $oD\acute{x} = 0$
 $\bar{o}L\acute{x} = 4 + 0 - 1 - 0 - 0 + 0 = 3$

FIG. 13-9 GIVEN $oL\acute{x}-1 = 4$ $oL\bar{x}-1 = 0$ $oDx = 0$ $oL\bar{x} = 0$ $oDx = 3$ $oD\acute{x} = 0$
 $\bar{o}L\acute{x} = 4 + 0 - 0 - 0 - 3 + 0 = 1$

FIG. 13-10 GIVEN $oL\acute{x}-1 = 1$ $oL\bar{x}-1 = 0$ $oDx = 0$ $oL\bar{x} = 0$ $oDx = 1$ $oD\acute{x} = 1$
 $\bar{o}L\acute{x} = 1 + 0 - 0 - 0 - 1 + 1 = 1$

STEP 35

$$\hat{o}L\acute{x} = oL\acute{x}-1 + oL\hat{x}-1 - oDx - oL\hat{x} - oL\acute{x}$$

SOLVE FOR $\hat{o}L\acute{x}$

EXAMPLES:

FIG. 13-1 GIVEN $oL\acute{x}-1 = 6$ $oL\hat{x}-1 = 0$ $oDx = 4$ $oL\hat{x} = 0$ $oL\acute{x} = 1$
 $\hat{o}L\acute{x} = 6 + 0 - 4 - 0 - 1 = 1$

FIG. 13-4 GIVEN $oL\acute{x}-1 = 3$ $oL\hat{x}-1 = 0$ $oDx = 1$ $oL\hat{x} = 0$ $oL\acute{x} = 0$
 $\hat{o}L\acute{x} = 3 + 0 - 1 - 0 - 0 = 2$

STEP 36

$$Q \frac{\overset{N}{\widehat{wLx}}}{\overset{N}{\widehat{wLx}}} \leq Fx - Fw - w^C x + G \quad \text{AND}$$

$$\overset{N}{\widehat{wLx}} \leq \overset{N}{\widehat{wLx-1}} - \overset{N}{\widehat{wDx}} \quad \text{BUT}$$

$$\text{WHEN } L\overset{N}{\widehat{w}} > 0 \quad \text{THEN}$$

$$\overset{N}{\widehat{wLx}} = 0$$

SOLVE FOR $\overset{N}{\widehat{wLx}}$

IN ALL FIGURES

$$Fw + Q \frac{\overset{N}{\widehat{wLx}}}{\overset{N}{\widehat{wLx}}} + w^C x \leq Fx + G$$

WHICH WHEN TRANSPOSED GIVES THE 1ST PART

EXAMPLES:

FIG. 17-1 GIVEN $Fx = 85$ $Fw = 145$ $w^C x = 4$

$$G = 75 \quad \overset{N}{\widehat{wLx-1}} = 1 \quad \overset{N}{\widehat{wDx}} = 0 \quad L\overset{N}{\widehat{w}} = 0$$

$$Q \frac{\overset{N}{\widehat{wLx-1}}}{\overset{N}{\widehat{wLx}}} \leq 85 - 145 - 4 + 75 = 11$$

$$\overset{N}{\widehat{wLx-1}} = 3 \quad \text{1ST PART}$$

$$\overset{N}{\widehat{wLx}} \leq 1 - 0 = 1 \quad \leftarrow \text{2ND PART}$$

THE DEVELOPMENT OF STEP 37

THE TIME OF PASSING LOCATION X FOR ALL CARS WILL BE DETERMINED AND FROM THIS WILL BE SUBTRACTED THE TIME THAT ALL CARS WERE DUE TO PASS LOCATION 1, ON THE ASSUMPTION THAT CARS WOULD NOT HAVE BEEN DELAYED AT 1. THIS DIFFERENCE GIVES THE ELAPSED TOTAL TIME IN TRAVELING FROM 1 THROUGH X WITH THE GIVEN SIGNAL TIMINGS AND OFFSETS. IF FROM THIS $N(i(x))$ IS SUBTRACTED THE RESULT IS THE TIME LOSS BECAUSE OF THE SIGNAL SYSTEM COMPARED TO UNINTERRUPTED FLOW.

THE CARS THAT ARE UNINTERRUPTED BY THE SIGNAL SYSTEM ARE THE oLx CARS. THESE WERE NOT DELAYED BY ANY SIGNAL. FOR CALCULATION THE oLx CARS ARE DESIGNATED AS $oLx = oLx^1 + oLx^2 + oLx^{\hat{}} + \bar{oLx} + \hat{oLx}$

t_{oLx^1}

SEE FIGURES 17-1 AND 20-1

$$\begin{aligned}
 t_{oLx^1} &= F_1 + G + \frac{C}{2N} - \frac{C}{N} (wLx^1) - \frac{C}{N} (1) + i(x + \\
 &F_1 + G + \frac{C}{2N} - \frac{C}{N} (wLx^2) - \frac{C}{N} (2) + i(x + \\
 &\dots + \\
 &F_1 + G + \frac{C}{2N} - \frac{C}{N} (wLx^{\hat{}}) - \frac{C}{N} (oLx^{\hat{}}) + i(x
 \end{aligned}$$

THEREFORE

$$t_{oLx^1} = oLx^1 [F_1 + G + i(x - \frac{C}{N}(wLx^1 - \frac{1}{2}))] - \frac{C}{N} [1+2+\dots+oLx^1]$$

t_{oLx^2}

SEE FIGURES 11-1 AND 11-2

$$\begin{aligned}
 t_{oLx^2} &= F_1 - (C-G) - \frac{C}{2N} + \frac{C}{N} (dx + \bar{w}Lx) + \frac{C}{N} (1) + i(x + \\
 &F_1 - (C-G) - \frac{C}{2N} + \frac{C}{N} (dx + \bar{w}Lx) + \frac{C}{N} (2) + i(x + \\
 &\dots + \\
 &F_1 - (C-G) - \frac{C}{2N} + \frac{C}{N} (dx + \bar{w}Lx) + \frac{C}{N} (oLx^2) + i(x
 \end{aligned}$$

THEREFORE

$$t_{oLx^2} = oLx^2 [F_1 + G + i(x - C + \frac{C}{N}(dx + \bar{w}Lx - \frac{1}{2}))] + \frac{C}{N} [1+2+\dots+oLx^2]$$

$\underline{t}^{\circ L \hat{x}}$

SEE FIGURES 11-1 AND 11-2

$$\begin{aligned} \underline{t}^{\circ L \hat{x}} &= F_1 + G + \frac{C}{2N} - \frac{C}{N}(N-ax) - \frac{C}{N}(1) + i^{\circ}x + \\ &F_1 + G + \frac{C}{2N} - \frac{C}{N}(N-ax) - \frac{C}{N}(2) + i^{\circ}x + \\ &\dots + \\ &F_1 + G + \frac{C}{2N} - \frac{C}{N}(N-ax) - \frac{C}{N}(\circ L \hat{x}) + i^{\circ}x \end{aligned}$$

THEREFORE

$$\underline{t}^{\circ L \hat{x}} = \circ L \hat{x} [F_1 + G + i^{\circ}x - \frac{C}{N}(N-ax - \frac{1}{2})] - \frac{C}{N} [1+2+\dots+\circ L \hat{x}]$$

$\underline{t}^{\circ L \hat{x}}$

SEE FIGURES 13-6 AND 13-9

$$\begin{aligned} \underline{t}^{\circ L \hat{x}} &= F_1 - (C-G) - \frac{C}{2N} + \frac{C}{N}(\circ 1x + \bar{w}Lx) + \frac{C}{N}(1) + i^{\circ}x + \\ &F_1 - (C-G) - \frac{C}{2N} + \frac{C}{N}(dx + \bar{w}Lx) + \frac{C}{N}(2) + i^{\circ}x + \\ &\dots + \\ &F_1 - (C-G) - \frac{C}{2N} + \frac{C}{N}(dx + \bar{w}Lx) + \frac{C}{N}(\circ L \hat{x}) + i^{\circ}x \end{aligned}$$

THEREFORE

$$\underline{t}^{\circ L \hat{x}} = \circ L \hat{x} [F_1 + G + i^{\circ}x - C + \frac{C}{N}(dx + \bar{w}Lx - \frac{1}{2})] + \frac{C}{N} [1+2+\dots+\circ L \hat{x}]$$

$\underline{t}^{\hat{\circ} L \hat{x}}$

SEE FIGURES 13-1 AND 13-4

$$\begin{aligned} \underline{t}^{\hat{\circ} L \hat{x}} &= F_1 + G + \frac{C}{2N} - \frac{C}{N}(N-ax) - \frac{C}{N}(1) + i^{\circ}x + \\ &F_1 + G + \frac{C}{2N} - \frac{C}{N}(N-ax) - \frac{C}{N}(2) + i^{\circ}x + \\ &\dots + \\ &F_1 + G + \frac{C}{2N} - \frac{C}{N}(N-ax) - \frac{C}{N}(\hat{\circ} L \hat{x}) + i^{\circ}x \end{aligned}$$

THEREFORE

$$\underline{t}^{\hat{\circ} L \hat{x}} = \hat{\circ} L \hat{x} [F_1 + G + i^{\circ}x - \frac{C}{N}(N-ax - \frac{1}{2})] - \frac{C}{N} [1+2+\dots+\hat{\circ} L \hat{x}]$$

$$t_{oLx} = t_{oL\acute{x}} + t_{oL\bar{x}} + t_{oL\hat{x}} + t_{\bar{o}L\acute{x}} + t_{\hat{o}L\acute{x}}$$

OR

$$\begin{aligned}
 t_{oLx} = & oL\acute{x} [F_1 + G + i(\bar{x} - \frac{C}{N} (\acute{w}L\acute{x} - \frac{1}{2}))] - \frac{C}{N} [1+2+\dots+oL\acute{x}] + \\
 & oL\bar{x} [F_1 + G + i(\bar{x} - C + \frac{C}{N} (dx + \bar{w}Lx - \frac{1}{2}))] + \frac{C}{N} [1+2+\dots+oL\bar{x}] + \\
 & oL\hat{x} [F_1 + G + i(\bar{x} - \frac{C}{N} (N - \alpha x - \frac{1}{2}))] - \frac{C}{N} [1+2+\dots+oL\hat{x}] + \\
 & \bar{o}L\acute{x} [F_1 + G + i(\bar{x} - C + \frac{C}{N} (dx + \bar{w}Lx - \frac{1}{2}))] + \frac{C}{N} [1+2+\dots+\bar{o}L\acute{x}] + \\
 & \hat{o}L\acute{x} [F_1 + G + i(\bar{x} - \frac{C}{N} (N - \alpha x - \frac{1}{2}))] - \frac{C}{N} [1+2+\dots+\hat{o}L\acute{x}]
 \end{aligned}$$

OR

$$\begin{aligned}
 t_{oLx} = & oLx [F_1 + G + i(\bar{x})] - oL\acute{x} [\frac{C}{N} (\acute{w}L\acute{x} - \frac{1}{2})] + [oL\bar{x} + \bar{o}L\acute{x}] [\frac{C}{N} (dx + \bar{w}Lx - \frac{1}{2}) - C] \\
 & [oL\hat{x} + \hat{o}L\acute{x}] [\frac{C}{N} (N - \alpha x - \frac{1}{2})] - [1+2+\dots+oL\acute{x}] + \frac{C}{N} [1+2+\dots+\bar{o}L\acute{x}] + \\
 & \frac{C}{N} [1+2+\dots+oL\bar{x}] - \frac{C}{N} [1+2+\dots+oL\hat{x}] - \frac{C}{N} [1+2+\dots+\hat{o}L\acute{x}]
 \end{aligned}$$

LET $1 + 2 + \dots + oL\acute{x} = \underline{oL\acute{x}}$ etc. THEN

$$\begin{aligned}
 t_{oLx} = & oLx [F_1 + G + i(\bar{x})] - \frac{C}{N} [\underline{oL\acute{x}} (\acute{w}L\acute{x} - \frac{1}{2}) - (oL\bar{x} + \bar{o}L\acute{x}) (dx + \bar{w}Lx - \frac{1}{2}) + \\
 & (oL\hat{x} + \hat{o}L\acute{x}) (N - \alpha x - \frac{1}{2})] + \underline{oL\acute{x}} - \underline{oL\bar{x}} - \underline{\bar{o}L\acute{x}} + \underline{oL\hat{x}} + \underline{\hat{o}L\acute{x}} \\
 & - C (oL\bar{x} + \bar{o}L\acute{x})
 \end{aligned}$$

WHICH GIVES THE SUM OF THE PASSING TIMES FOR ALL THE oLx CARS.

EXAMPLE:

FIG. 13-1

$$\begin{aligned}
 \text{GIVEN } & oLx = 2 \quad F_1 = 45 \quad G = 75 \quad i(\bar{x}) = 10 \quad \frac{C}{N} = 10 \quad oL\acute{x} = 1 \\
 & \acute{w}L\acute{x} = 0 \quad oL\bar{x} = 0 \quad \bar{o}L\acute{x} = 0 \quad dx = 0 \quad \bar{w}Lx = 4 \quad oL\hat{x} = 0 \\
 & \hat{o}L\acute{x} = 1 \quad N = 10 \quad \alpha x = 5
 \end{aligned}$$

$$t_{oLx} = 2 [45+75+10] - 10 [1(0-\frac{1}{2}) - (0+0) (0+4-\frac{1}{2}) + (0+1) (10-5-\frac{1}{2}) + 1 - 0 + 1]$$

$$t_{oLx} = 200$$

LET $d^5 + d^6 + d^7 + d^8 = 5d^8$

$$xLx = Dx + dx$$

$$\ddot{x}Lx = dx$$

THE t FOR THE CARS ORIGINATING FROM LOCATIONS OTHER THAN 0 IS DEVELOPED AS FOLLOWS:

SEE FIGURE 24-1

$$\begin{aligned} t_{wLu} &= Fw + d \frac{wD^{\bar{}} + wd + 1}{w} + w(u + \\ &Fw + d \frac{wD^{\bar{}} + wd + 2}{w} + w(u + \\ &+ \dots \dots + \\ &Fw + d \frac{wD^{\bar{}} + wd + wLu}{w} + w(u \\ &- \ddot{w}Lu (c) \end{aligned}$$

LET (FOR THIS STEP ONLY) $w =$ ANY LOCATION
1 TO x INCLUSIVE. THEN

$$t_{wLx} = wLx (Fw + w(x) + \frac{wD^{\bar{}} + wd + 1}{w} d \frac{wD^{\bar{}} + wd + wLx}{w} - c (\ddot{w}Lx))$$

WHERE

$$wD = 0 \quad wd = 0$$

$wD^{\bar{}}$ = THE CARS ORIGINATING AT w , DELAYED INDIRECTLY AT LOCATIONS $w + 1, w + 2, w + 3$, AND SO FORTH AND PASSING x DURING THE G FOLLOWING Fx

wd IS SIMILAR EXCEPT THEY PASS x DURING THE G PRECEDING Fx .

$$t_{Lx} = t_{oLx} + t_{wLx} \quad \text{OR}$$

STEP 37

$$\begin{aligned} \underline{tLx} = & wLx (Fw + w(x) + \frac{w\bar{D}+wd+1}{\alpha} \alpha \frac{w\bar{D} + wd + wLx}{\alpha} - C (\bar{w}Lx) \\ & + oLx (F_1 + G + i(x) - \frac{C}{N} [oLx' (\bar{w}Lx' - \frac{1}{2}) - (oLx\bar{+}\bar{o}Lx') (dx + \bar{w}Lx - \frac{1}{2}) \\ & + (oLx\hat{+}\hat{o}Lx') (N - \alpha x - \frac{1}{2}) + \underline{oLx} - \underline{oLx\bar{+}} - \underline{\bar{o}Lx'} + \underline{oLx\hat{+}} + \underline{\hat{o}Lx'}] \\ & - C (oLx\bar{+} + \bar{o}Lx') \end{aligned}$$

IN MOST COMPLEX SYSTEMS LINES 2, 3 AND 4 WILL BE EQUAL TO ZERO BECAUSE THERE WILL BE NO CARS TO TRAVEL THE ENTIRE DISTANCE WITHOUT DELAY.

EXAMPLE:

FIG. 17-1

GIVEN ${}_1Lx = 1, {}_2Lx = 3, {}_3Lx = 1, {}_4Lx = 4, F_1 = 45, F_2 = 95, F_3 = 145, F_4 = 85, {}_1(x) = 10, {}_2(x) = 6, {}_3(x) = 4, {}_4(x) = 0, {}_1\bar{D} = 0, {}_2\bar{D} = 0, {}_3\bar{D} = 0, {}_4\bar{D} = 0, {}_1d = 0, {}_2d = 0, {}_3d = 0, {}_4d = 0, C = 100, {}_1'Lx = 0, {}_2'Lx = 0, {}_3'Lx = 0, oLx = 1, G = 75, N = 10, oLx' = 1, \bar{w}Lx' = 1, oLx\bar{+} = 0, \bar{o}Lx' = 0, dx = 0, \bar{w}Lx = 1, oLx\hat{+} = 0, \hat{o}Lx' = 0, \alpha x = 1$

$$\begin{aligned} \underline{tLx} = & 1(45+10) + \frac{0+0+1}{\alpha} \alpha \frac{0+0+1}{\alpha} - 100 (0) + \\ & 3(95+6) + \frac{0+0+1}{\alpha} \alpha \frac{0+0+3}{\alpha} - 100 (0) + \\ & 1(145+4) + \frac{0+0+1}{\alpha} \alpha \frac{0+0+1}{\alpha} - 100 (0) + \\ & 4(85+0) + \frac{0+0+1}{\alpha} \alpha \frac{0+0+4}{\alpha} - 100 (0) + \\ & 1(45+75+10) - \frac{100}{10} [1(1-\frac{1}{2}) - (0+0) (0+1-\frac{1}{2}) + \\ & (0+0) (10-1-\frac{1}{2}) + 1 - 0 - 0 + 0 + 0] \end{aligned}$$

THEREFORE

$$\begin{aligned} \underline{tLx} = & 55 + 5 - 0 + 303 + 23 - 0 + 149 + 5 - 0 + 340 + 35 - 0 + \\ & 130 - 10 [\frac{1}{2} - 0 + 0 + 1 - 0 + 0] \end{aligned}$$

THEREFORE

$$\underline{tLx} = 1045 - 15 = 1030$$

STEP 38

$$t^L = N \left(F_1 + G + \frac{C}{2N} \right) - \frac{C}{N} (LN)$$

SOLVE FOR t^L

IN FIGURE 1-1

$$\begin{aligned} t^L &= F_1 + G + \frac{C}{2N} - \frac{C}{N} (1) + \\ &F_1 + G + \frac{C}{2N} - \frac{C}{N} (2) + \\ &+ \dots + \dots + \\ &F_1 + G + \frac{C}{2N} - \frac{C}{N} (N) \qquad \text{OR} \\ t^L &= N \left(F_1 + G + \frac{C}{2N} \right) - \frac{C}{N} (LN) \end{aligned}$$

EXAMPLE:

FIG. 1-1

GIVEN $N = 6$ $F_1 = 90$ $G = 40$ $C = 60$

$$t^L = 6(90 + 40 + 5) - 10 (21)$$

$$t^L = 600$$

STEP 1

oD_1

$$\frac{C}{N} (oD_1) - Q \frac{oD_1}{2N} < (C - G) + \frac{C}{2N}$$

STEP 2

H_1

$$H_1 = \left(\begin{array}{l} Q \frac{oD_1}{2N} \\ G - \frac{C}{2N} \end{array} \right) \text{ OR } \left. \begin{array}{l} \\ \end{array} \right\} \text{ USE LARGER}$$

STEP 3

oL_1

$oL_1 = N - oD_1$

ALL ELEMENTS TO LOCATION 1 OTHER THAN oD_1 , H_1
AND oL_1 ARE EQUAL TO ZERO.

STEP 4

F_u

$F_u \geq F_{u-1} + H_{u-1} + u-1 C_u - G$ AND

$F_u < F_{u-1} + H_{u-1} + u-1 C_u - G + C$ BUT

$F_u = F'_u + MC$

STEP 5

$\acute{w}P_u$

$$\alpha \frac{\acute{w}D\bar{v} + \acute{w}dv + \acute{w}P_u}{\acute{w}P_u} \leq Fu - Fw - w\bar{c}_u - (C - G) \text{ AND}$$

$$\acute{w}P_u \leq \acute{w}L_{u-1} \text{ BUT WHEN}$$

$$Fw + Q^L + w\bar{c}_u \Rightarrow Fu - (C-G) \text{ THEN}$$

$$\acute{w}P_u = 0$$

STEP 6

$\acute{\acute{w}}P_u$

$$\alpha \frac{Dw + \acute{\acute{w}}dv + \acute{\acute{w}}P_u}{\acute{\acute{w}}P_u} \leq Fu - Fw - w\bar{c}_u + G \text{ AND}$$

$$\acute{\acute{w}}P_u \leq \acute{\acute{w}}L_{u-1} \text{ AND WHEN}$$

$$dw = 0 \text{ THEN}$$

$$\acute{\acute{w}}P_u = 0$$

STEP 7

$\acute{w}D\bar{u}$

WHEN $Fu \leq Fw + w\bar{c}_u$ THEN

$\acute{w}D\bar{u} = 0$ BUT

WHEN $Fu > Fw + w\bar{c}_u$ THEN

$\acute{w}D\bar{u} = \bar{w}L_{u-1} (1 - wP_u)$

STEP 8

$\acute{\acute{w}}D\bar{u}$

WHEN $dw = 0$ THEN

$\acute{\acute{w}}D\bar{u} = 0$ BUT

WHEN $dw > 0$ THEN

$\acute{\acute{w}}D\bar{u} = \bar{w}L_{u-1} (1 - wP_u)$

STEP 9		$\frac{\Delta}{wDu}$
WHEN	$F_u \leq F_w + wC_u$	THEN
	$\frac{\Delta}{wDu} = 0$	BUT
WHEN	$F_u > F_w + wC_u$	THEN
	$\frac{\Delta}{wDu} = \bar{w}L_{u-1} - wP_u$	AND WHEN
	$\bar{w}L_{u-1} = 0$	THEN $\frac{\Delta}{wDu} = 0$

STEP 10		$\frac{\Delta}{wDu}$
WHEN	$dw = 0$	THEN
	$\frac{\Delta}{wDu} = 0$	BUT
WHEN	$dw > 0$	THEN
	$\frac{\Delta}{wDu} = \bar{w}L_{u-1} - wP_u$	

STEP 11		oP_u^{Δ}
	$oP_u^{\Delta} \leq \frac{N}{C} (F_u - F_1 - i(u)) + \frac{1}{2} - wP_u - oL_{u-1}^{\bar{u}} - oL_{u-1}^{\bar{u}}$	AND
	$oP_u^{\Delta} \leq oL_{u-1}^{\bar{u}} + oL_{u-1}^{\bar{u}}$	BUT WHEN $oP_{u-1}^{\Delta} = 0$
	THEN $oP_u^{\Delta} = 0$	

STEP 12		$oP_u^{\bar{u}}$
	$oP_u^{\bar{u}} \leq \frac{N}{C} (F_u - F_1 - i(u)) + \frac{1}{2} - wP_u - 2 oP_u^{\Delta}$	AND
	$oP_u^{\bar{u}} \leq oL_{u-1}^{\bar{u}} + oL_{u-1}^{\bar{u}}$	BUT
WHEN	$oP_u^{\Delta} = 0$	THEN
	$oP_u^{\bar{u}} = 0$	

STEP 13		oP_u^{\wedge}
$oP_u^{\wedge} \leq \frac{N}{C} (F_u - F_l - i(u)) + \frac{1}{2} - wP_u - \bar{w}D_u^{\wedge}$	AND	
$oP_u^{\wedge} \leq \left\{ \begin{array}{l} (oL_u^{\wedge} - 1 \text{ OR}) \\ (oL_u^{\wedge} - 1) \end{array} \right\}$	USE LARGER	BUT
WHEN $oP_u^{\wedge} > 0$		THEN
$oP_u^{\wedge} = 0$		

STEP 14		Q_u
$Q_u = wP_u + oP_u$		

STEP 15		$\acute{w}D_u^{\bar{}}$
$Q \frac{\acute{w}D_v^{\bar{}} + \acute{w}d_v + \acute{w}D_u^{\bar{}}}{} - Q \frac{Q_w - Q_u + \acute{w}D_v^{\bar{}} + \acute{w}d_v + \acute{w}D_u^{\bar{}}}{} < F_u - F_w - wC_u$		
AND	$\acute{w}D_u^{\bar{}} \leq \acute{w}L_u - 1$	BUT WHEN $Q_u \geq Q_w$ THEN
$\acute{w}D_u^{\bar{}} = 0$	AND WHEN $F_w + Q \frac{\acute{w}D_v^{\bar{}} + \acute{w}d_v + 1}{} + wC_u \geq F_u +$	
$Q \frac{Q_w - Q_u + \acute{w}D_v^{\bar{}} + \acute{w}d_v + 1}{}$	THEN	$\acute{w}D_u^{\bar{}} = 0$

STEP 16		$\acute{w}D_u^{\bar{}}$
WHEN	$F_u \leq F_w + wC_u$	THEN
	$\acute{w}D_u^{\bar{}} = 0$	AND
WHEN	$F_u > F_w + wC_u$	THEN
	$\acute{w}D_u^{\bar{}} = \acute{w}L_u - 1 - wP_u - \bar{w}D_u^{\bar{}}$	

STEP 17

$$\frac{C}{N} (oD\bar{u}) - Q \frac{\bar{w}D\hat{u} + oD\bar{u}}{\bar{w}D\hat{u} + oD\bar{u}} < Fu - Fi - iCu + \frac{C}{2N} + (C-G) -$$

$$\frac{C}{N} (Qu + \bar{w}D\hat{u}) \quad \text{AND}$$

$$oD\bar{u} \leq oL\bar{u} - 1 - oP\bar{u}$$

STEP 18

$$\frac{C}{N} (oD\hat{u}) - Q \frac{wDu + oD\hat{u}}{wDu + oD\hat{u}} < Fu - Fi - iCu + \frac{C}{2N} + (C-G) -$$

$$\frac{C}{N} (Qu - 1 - oL\hat{u} - 1) \quad \text{AND}$$

$$oD\hat{u} \leq oL\hat{u} - 1 - oP\hat{u}$$

STEP 19

$$\frac{C}{N} (oD\acute{u}) - Q \frac{\bar{w}D\hat{u} + oD\acute{u}}{\bar{w}D\hat{u} + oD\acute{u}} < Fu - Fi - iCu + \frac{C}{2N} + (C-G) -$$

$$\frac{C}{N} (Qu + \bar{w}D\hat{u}) \quad \text{AND}$$

$$oD\acute{u} \leq oL\acute{u} - 1 - oP\acute{u}$$

STEP 20

$$\frac{C}{N} (oD\acute{u}) - Q \frac{wD\bar{u} + wD\bar{u} + oD\acute{u}}{wD\bar{u} + wD\bar{u} + oD\acute{u}} < Fu - Fi - iCu + \frac{C}{2N} +$$

$$(C-G) - \frac{C}{N} (Qu + wD\bar{u} + wD\bar{u}) \quad \text{AND}$$

$$oD\acute{u} \leq N - Qu - wDu \quad \text{BUT WHEN } oL\acute{u} - 1 = 0 \quad \text{THEN}$$

$$oD\acute{u} = 0$$

STEP 21

Du

$$Du = \hat{w}Du + \overset{\wedge\wedge}{w}Du + wD\bar{u} + oD\bar{u} + oD\hat{u} + oD\acute{u} + oD\acute{u}$$

STEP 22

Hu

$$Hu = \left\{ \begin{array}{l} \alpha \frac{Du}{Hu-1 - Fu + Fu-1 + u-1Cu} \quad \text{OR} \\ \text{USE LARGER} \end{array} \right\}$$

STEP 23

wdu

$$\alpha \frac{wdu}{wdu} - \alpha \frac{Du + \alpha w + wdu}{wdu} < Fu - Fw - wCu - C \quad \text{AND}$$

$$\begin{array}{l} wdu = wPu \\ Fw + \alpha^L + wCu \Rightarrow Fu - C + \alpha \frac{Du + \alpha w + 1}{wdu} \quad \text{BUT WHEN THEN} \\ wdu = 0 \end{array}$$

STEP 24

wdu

$$\alpha \frac{Dw + wdu}{wdu} - \alpha \frac{Du + wdu}{wdu} < Fu - Fw - wCu \quad \text{AND}$$

$$\begin{array}{l} wdu \leq wPu \\ dw = 0 \quad \text{THEN} \quad wdu = 0 \\ \text{WHEN } \alpha \frac{Du}{wdu} - \alpha \frac{Dw}{wdu} \leq Fu - Fu + wCu \quad \text{THEN} \quad wdu = 0 \end{array}$$

STEP 25

odu

$$\frac{C}{N} (odu) - \alpha \frac{Du + wdu + odu}{odu} < Fu - Fi - iCu + \frac{C}{2N} - G -$$

$$\frac{C}{N} (wdu) \quad \text{AND}$$

$$odu \leq oP\bar{u} + oP\acute{u}$$

<p>STEP 26</p> $\acute{w}L\acute{u} = \acute{w}Pu - \acute{w}du$	$\acute{w}L\acute{u}$
--	-----------------------

<p>STEP 27</p> $\acute{w}L\acute{u} = \acute{w}Pu - \acute{w}du$	$\acute{w}L\acute{u}$
--	-----------------------

<p>STEP 28</p> $\acute{w}L\acute{u} = \acute{w}Lu-1 - \acute{w}Du - \acute{w}Pu$	$\acute{w}L\acute{u}$
--	-----------------------

<p>STEP 29</p> $D\bar{u} = \bar{w}D\bar{u} + \acute{w}D\bar{u} + oD\bar{u} + oD\bar{u}$	$D\bar{u}$
<p>WHEN $\bar{w}D\bar{u} = 0$</p>	<p>BUT</p>
<p>$D\bar{u} = 0$</p>	<p>THEN</p>

<p>STEP 30</p>	$\bar{w}Lu$
$\bar{w}Lu = \bar{w}Lu-1 - wDu + \acute{w}D\bar{u}$	<p>BUT WHEN $wdu > 0$ THEN</p>
$\bar{w}Lu = 0$	<p>AND WHEN</p>
$\bar{w}Lu-1 = 0$	<p>THEN $\bar{w}Lu = 0$</p>

STEP 31	$oL\vec{u}$
$oL\vec{u} = oP\vec{u} - odu$	

STEP 32	$oL\hat{u}$
$oL\hat{u} = oP\hat{u}$	

STEP 33	$oL\acute{u}$
$oL\acute{u} = N - a_u - Du - wL\acute{u}$	

STEP 33 A	$oL\acute{u}$
$oL\acute{u} = oP\acute{u} - odu$	

STEP 34	$\vec{o}L\acute{x}$
$\vec{o}L\acute{x} = oL\acute{x}_{-1} + oL\vec{x}_{-1} - odx - oL\vec{x} - oDx + oD\acute{x}$	

STEP 35	$\hat{o}L\acute{x}$
$\hat{o}L\acute{x} = oL\acute{x}_{-1} + oL\hat{x}_{-1} - oDx - oL\hat{x} - oL\acute{x}$	

STEP 36	$\acute{w}L\acute{x}$
$\acute{d} \frac{\acute{w}L\acute{x}}{\acute{w}L\acute{x}} \leq Fx - Fw - w(\acute{x} + G$	AND
$\frac{\acute{w}L\acute{x}}{\acute{w}L\acute{x}} \leq \acute{w}L\acute{x}-1 - \acute{w}D\bar{x}$	BUT
WHEN $L\acute{w} > 0$	THEN
$\acute{w}L\acute{x} = 0$	

STEP 37	$\dagger Lx$
$\dagger Lx = wLx (Fw+w(\acute{x}) + \frac{wD\bar{w}+1}{wD\bar{w}+1} \acute{d} \frac{wD\bar{w}+1}{wD\bar{w}+1} Lx$ $- C (\acute{w}Lx) + oLx (F_1+G_1(\acute{x}) - \frac{C}{N} [oL\acute{x}(\acute{w}L\acute{x}-\frac{1}{2})$ $- (oL\bar{x}+\bar{o}L\acute{x}) (dx+\bar{w}Lx-\frac{1}{2}) + (oL\hat{x}+o\hat{L}\acute{x}) (N-\alpha x-\frac{1}{2})$ $+ \frac{oL\acute{x}}{oL\bar{x}} - \frac{oL\bar{x}}{\bar{o}L\acute{x}} + \frac{oL\hat{x}}{oL\acute{x}} + \frac{o\hat{L}\acute{x}}{oL\bar{x}}]$ $- C (oL\bar{x} + \bar{o}L\acute{x})$	

STEP 38	$\dagger \perp$
$\dagger \perp = N (F_1+G+\frac{C}{2N}) - \frac{C}{N} (\perp N)$	

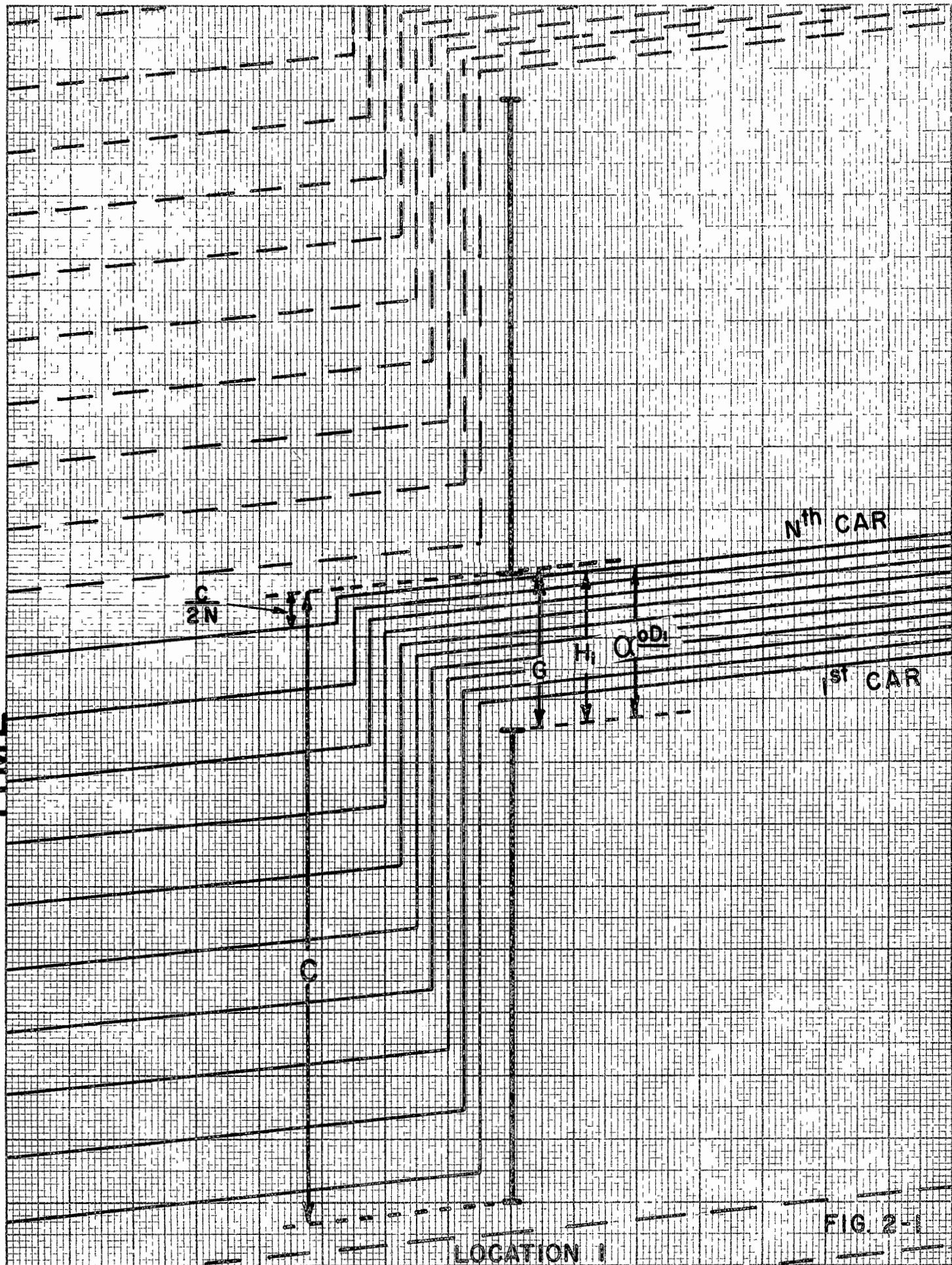
STEP 39	$\perp \dagger x$
$\perp \dagger x = \dagger Lx - \dagger \perp$	

STEP 40	$\perp \top x$
$\perp \top x = \perp \dagger x - N (i(\acute{x}))$	



TIME

KEUFFEL & ESSER CO



DISTANCE

LOCATION 1

Nth CAR

1st CAR

FIG. 2-1

DISTANCE

TIME

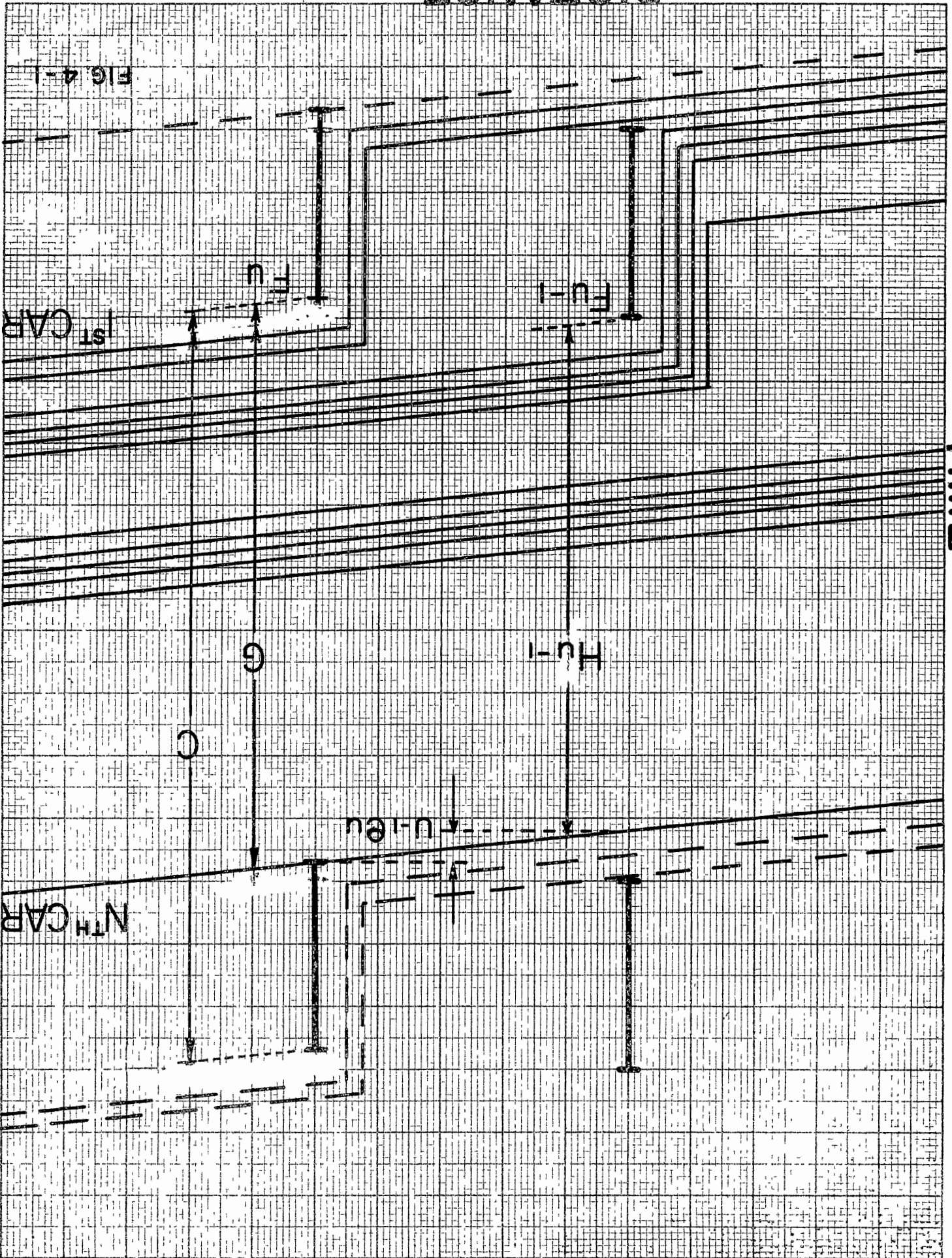


FIG 4-1

9a

TIME

DISTANCE

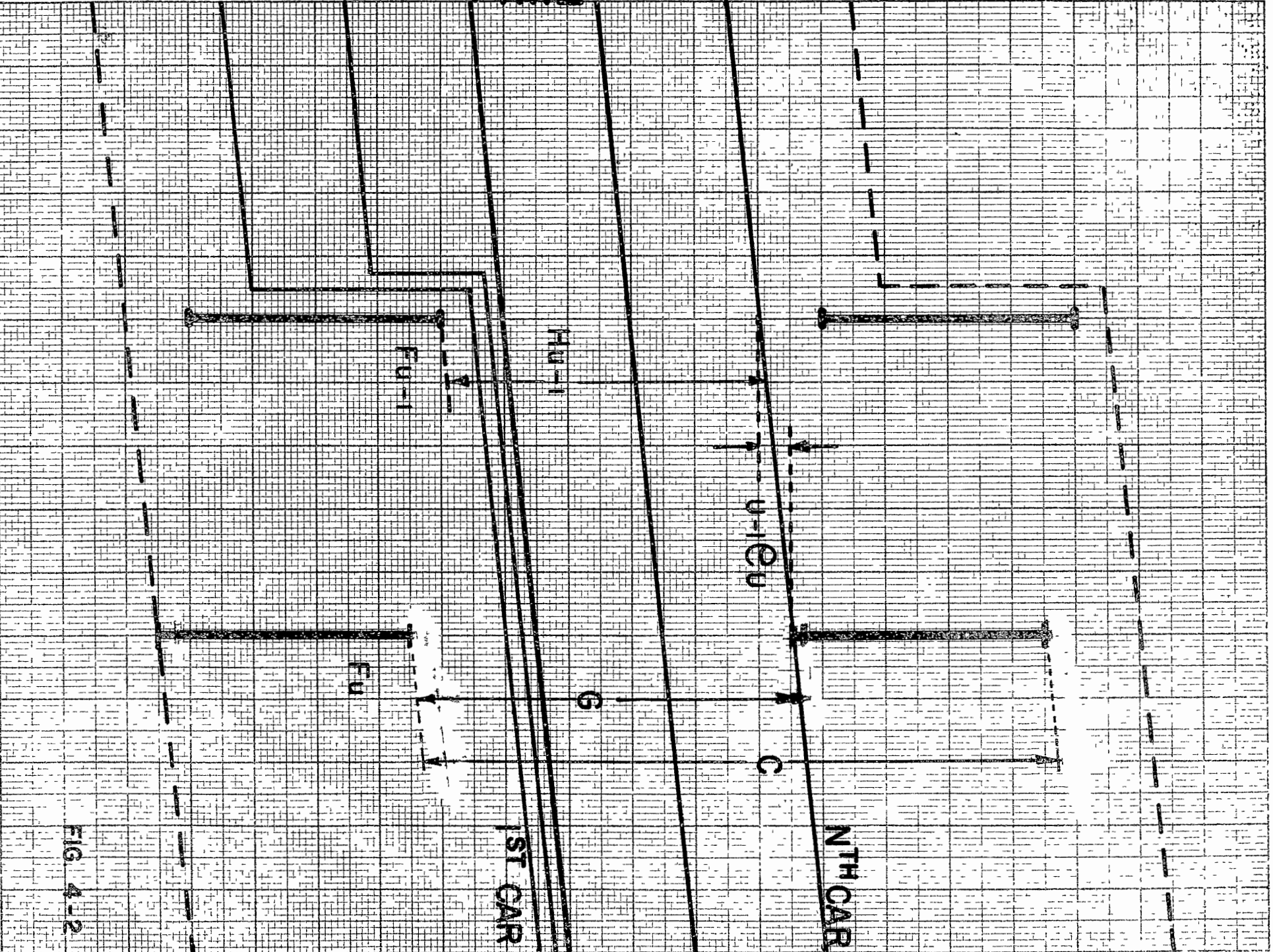


FIG. 4-2

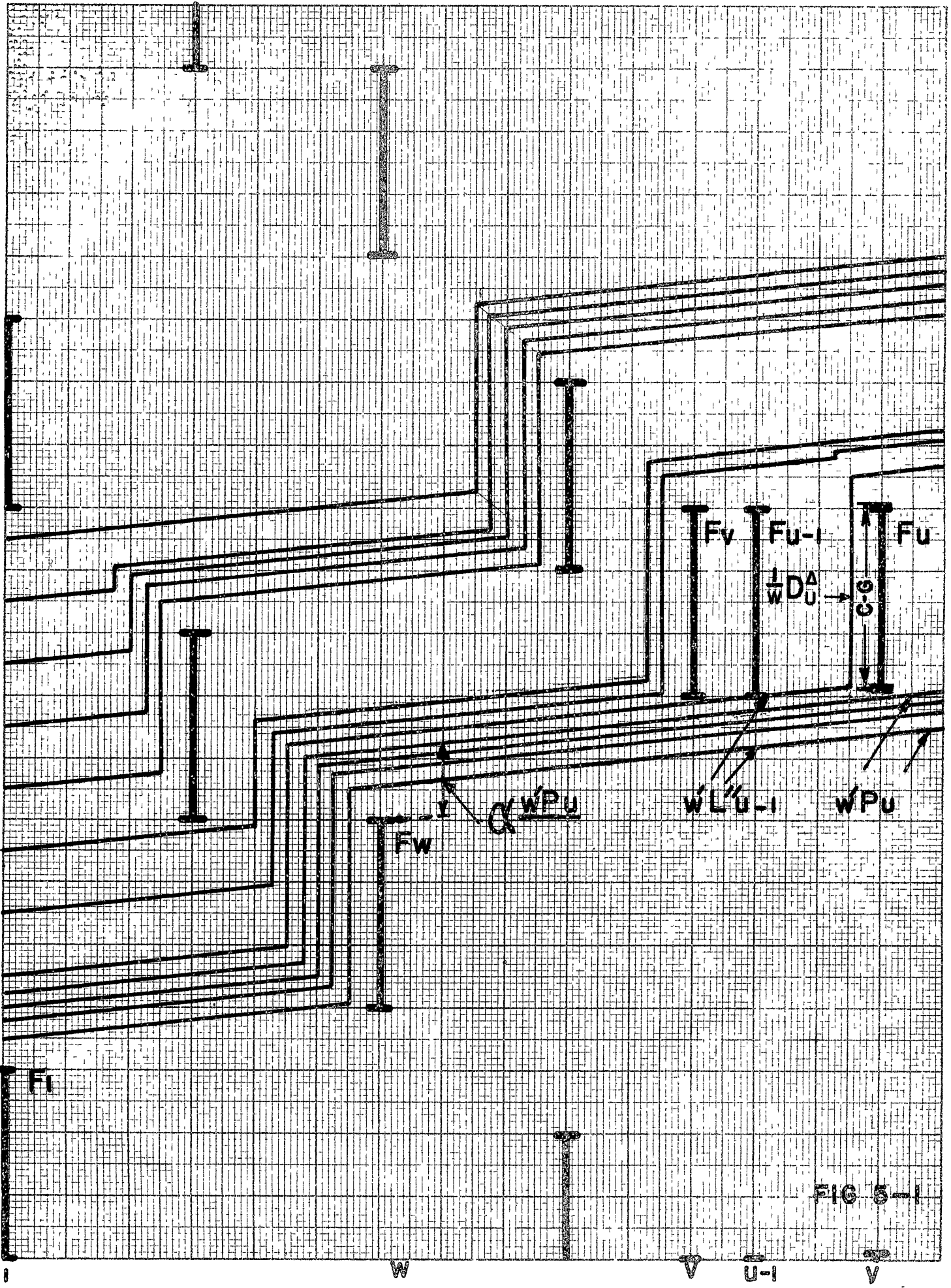


FIG 5-1

K&E 10 X 10 TO 1/2 INCH 46 1472
7 1/2 X 10 INCHES MADE IN U.S.A.
KEUFFEL & ESSER CO

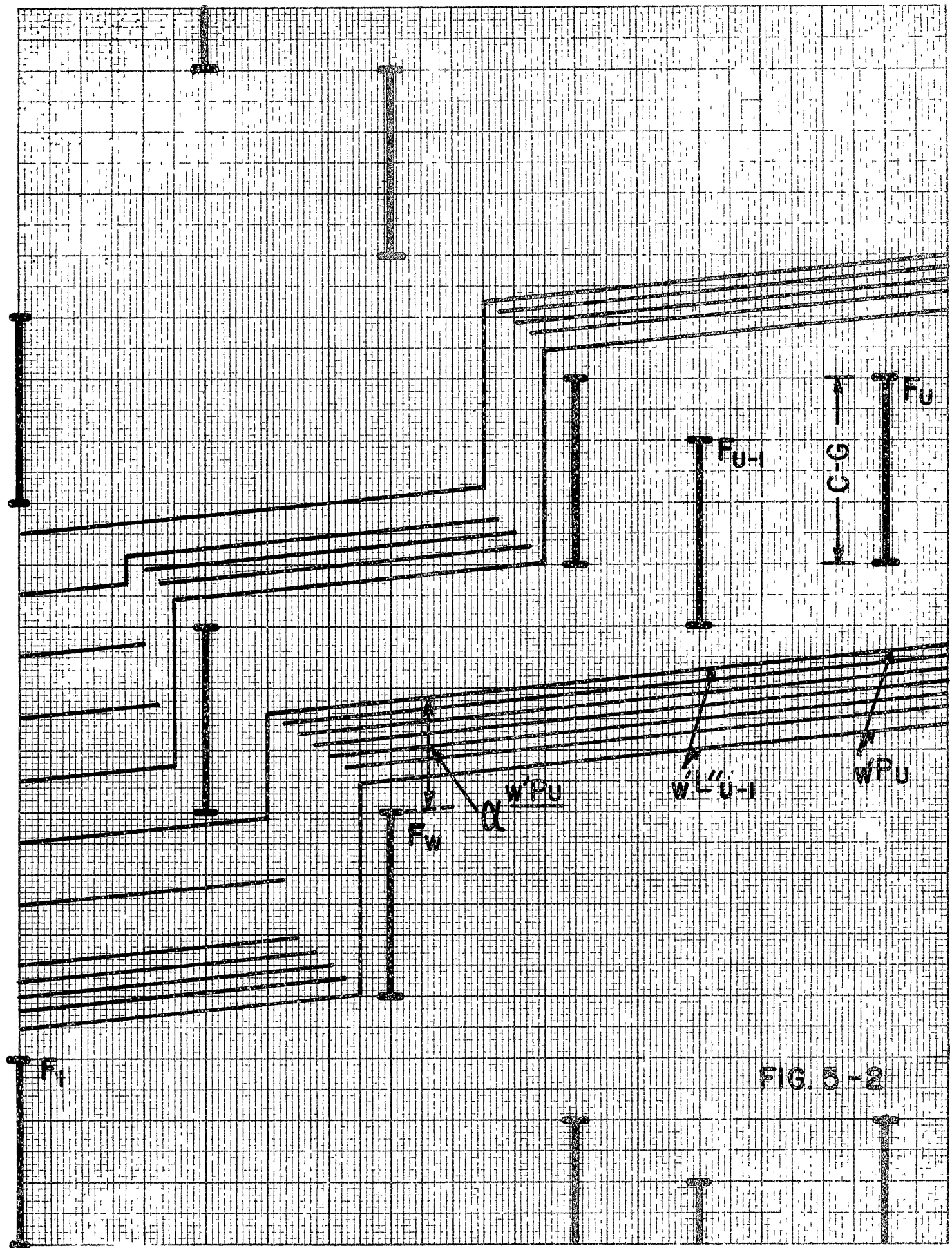


FIG. 5 - 2

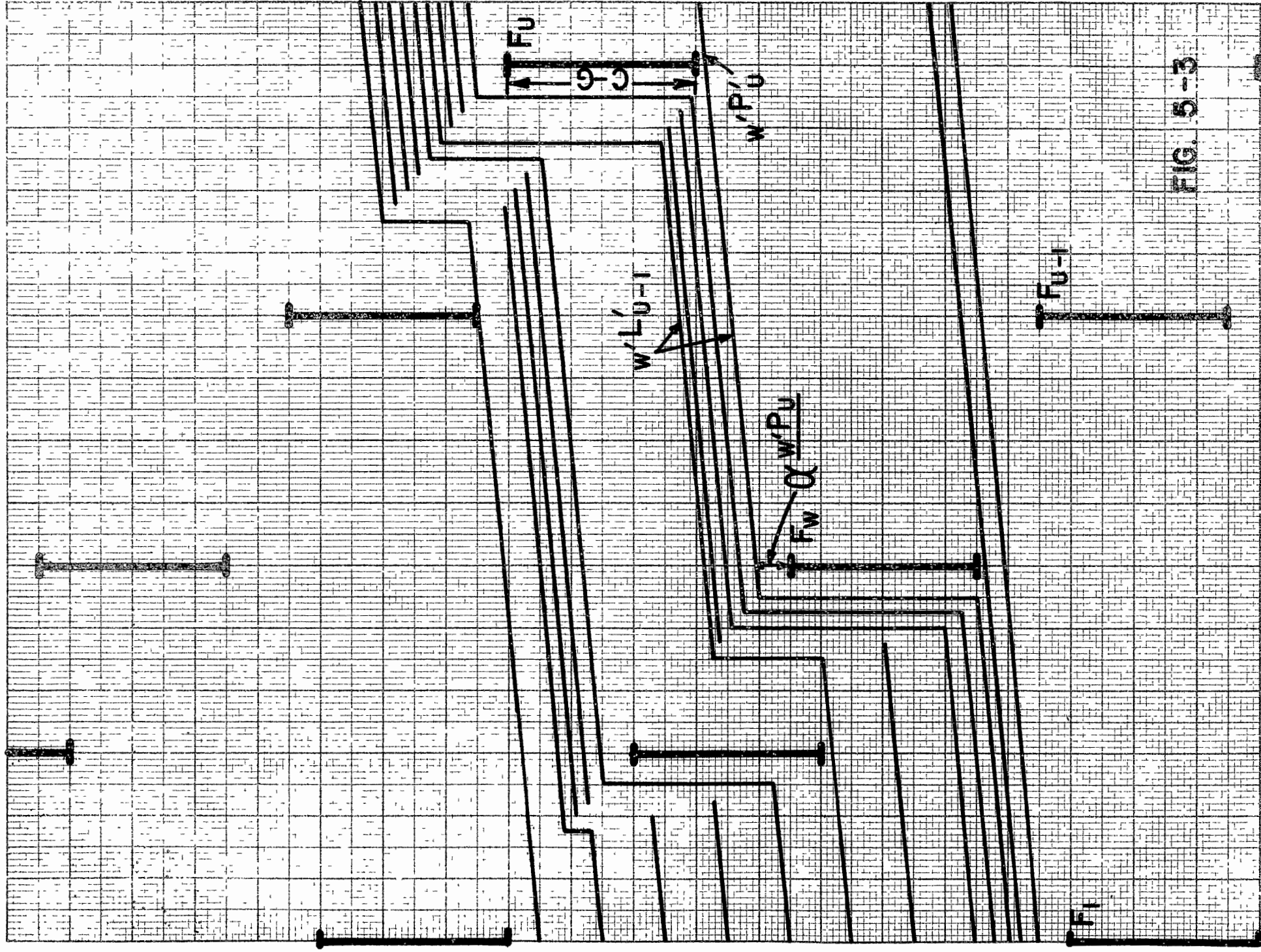


FIG. 5-3

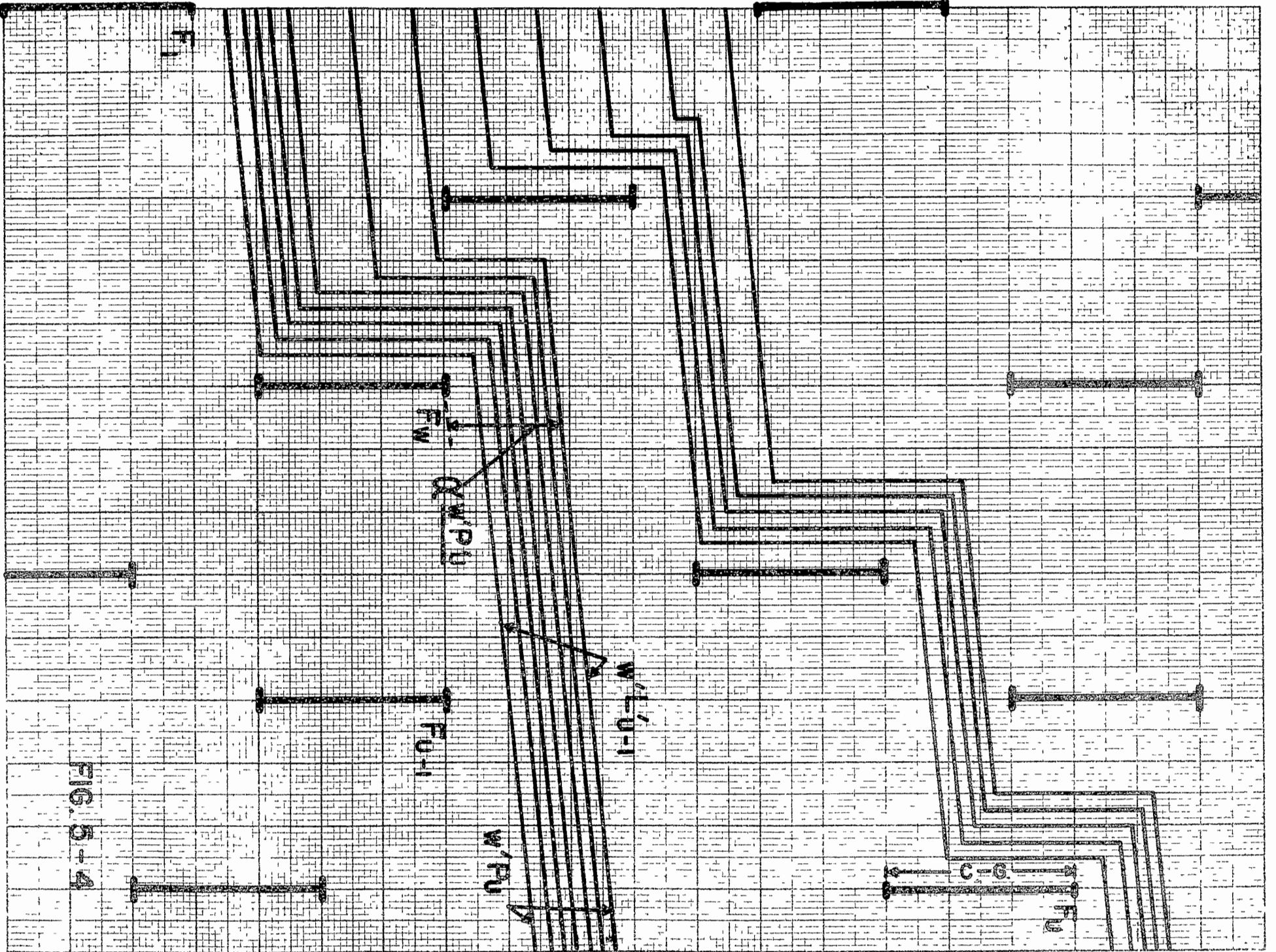


FIG. 5-4

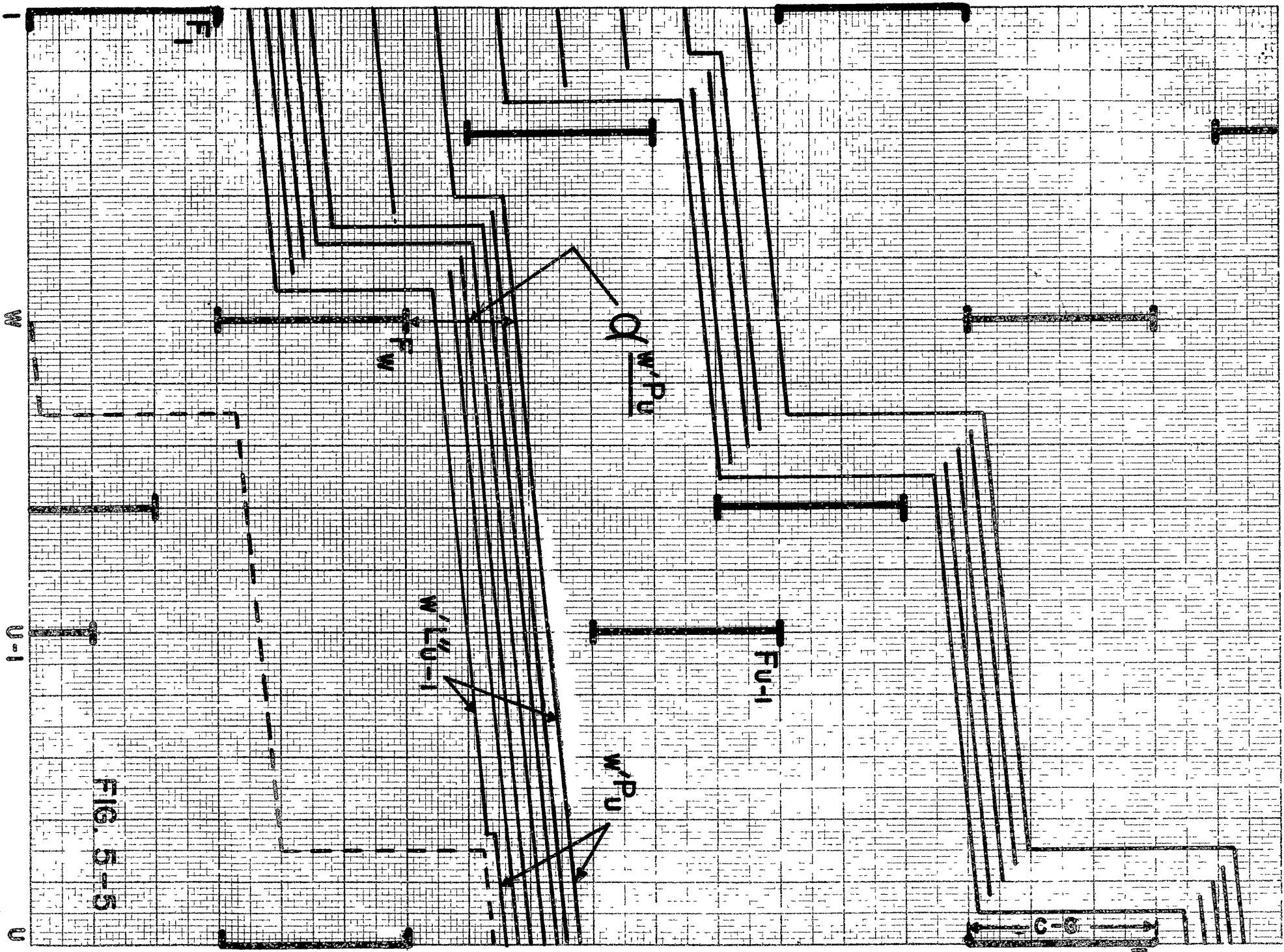


FIG. 5-5

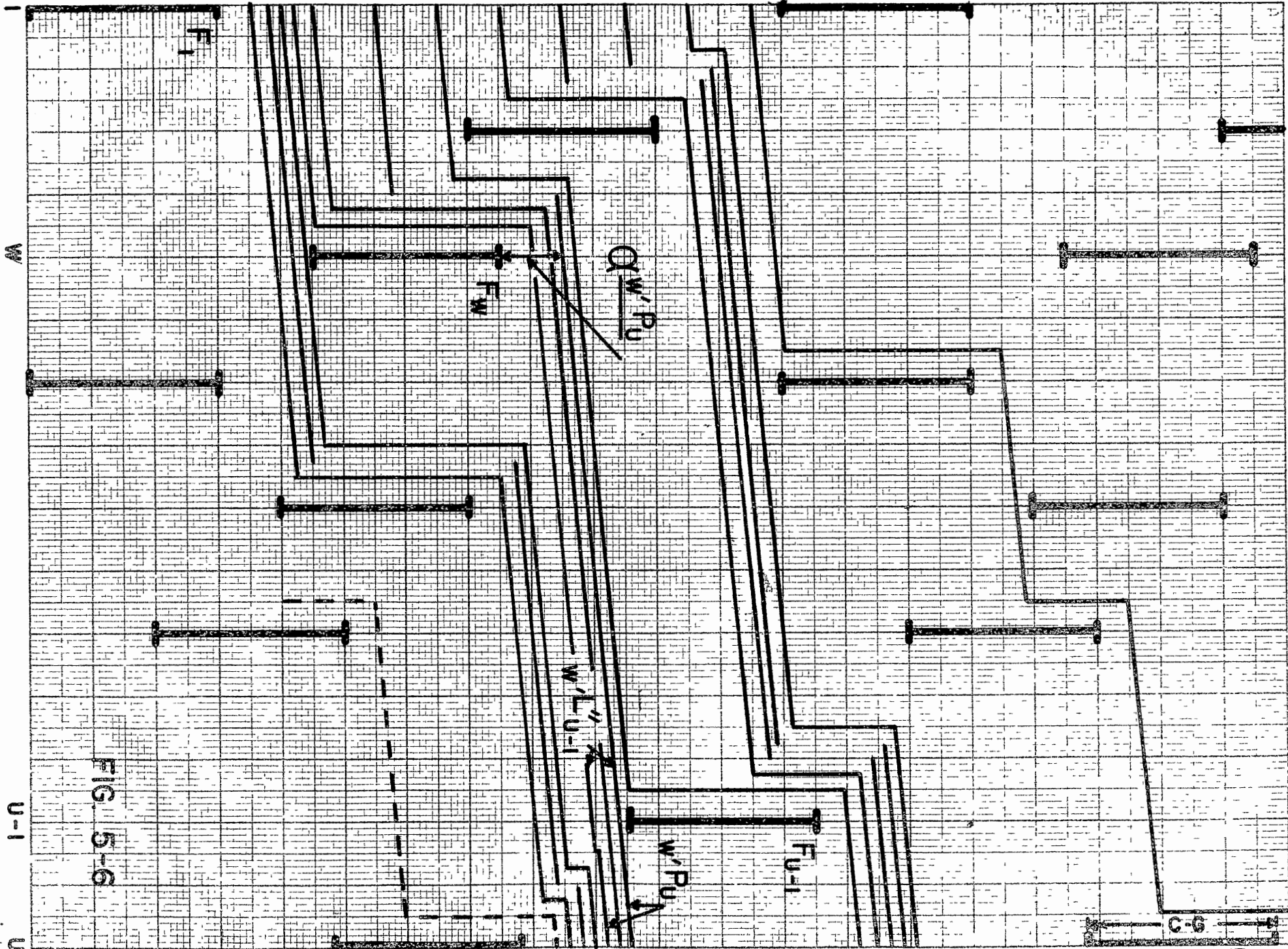


FIG. 5-6

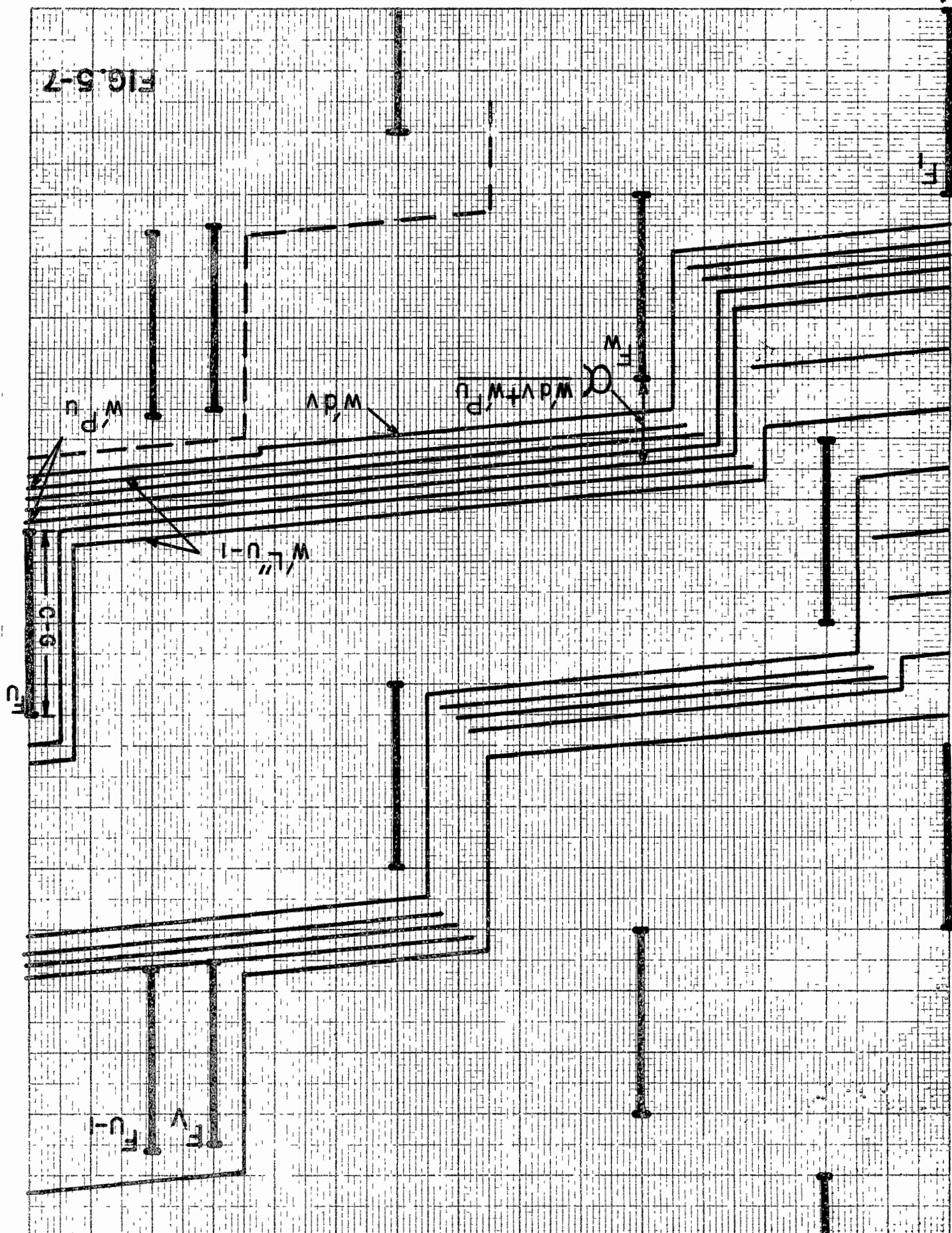
11/1

12-5-7
U

V U-1

W

FIG. 5-7



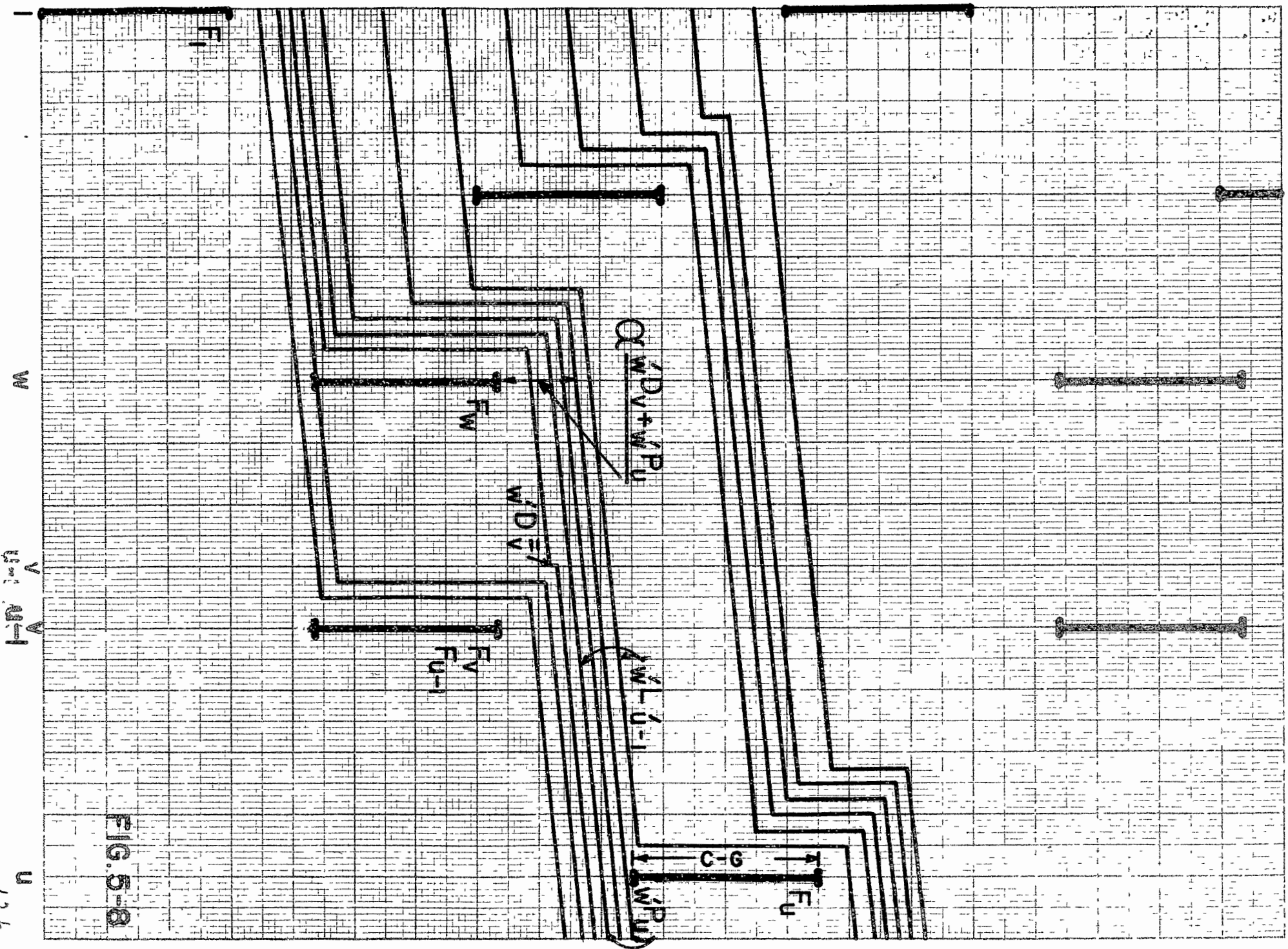


FIG. 5-8

U-1
7
8

6

5

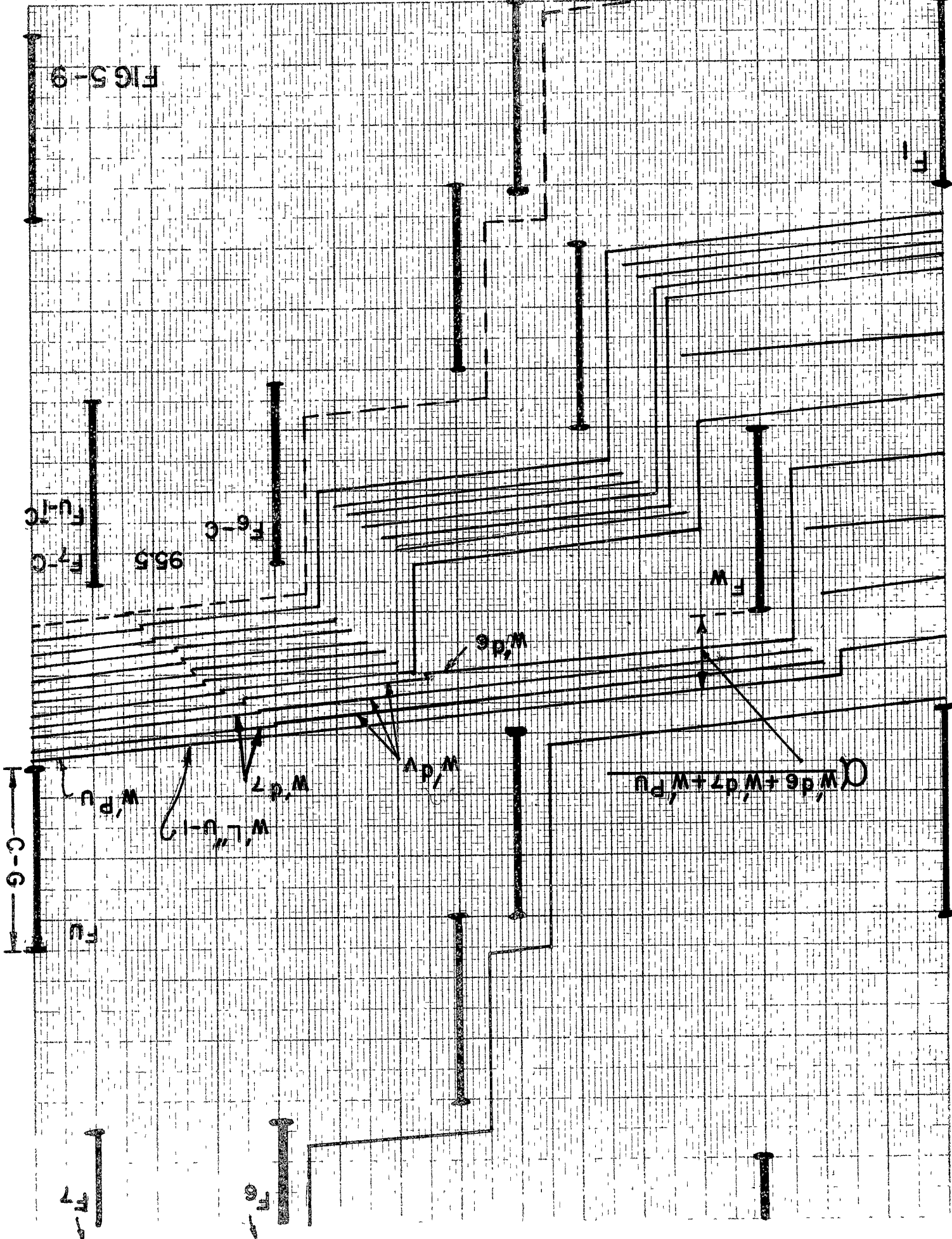
4

3

W

1

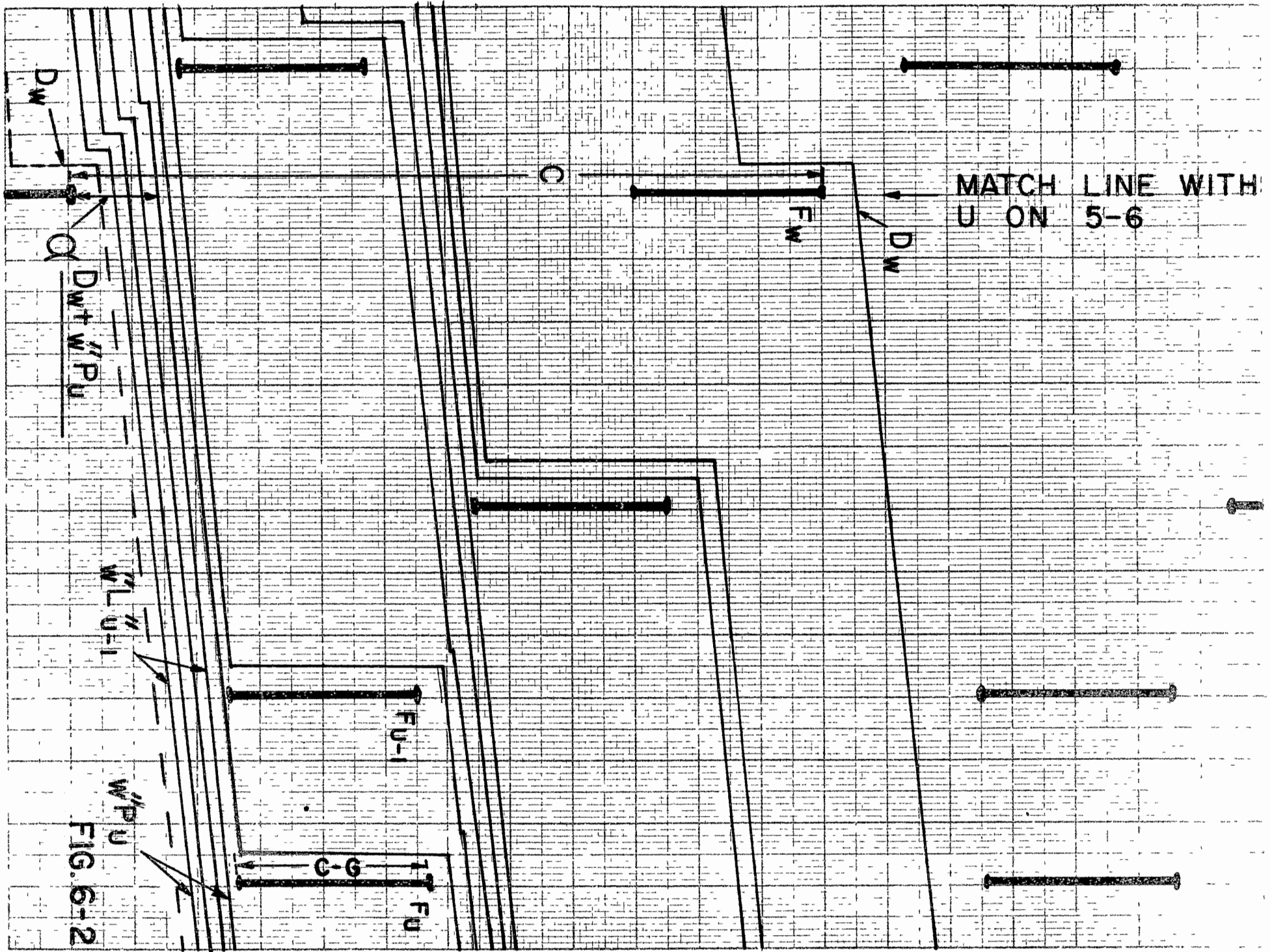
FIG 5-9



7

8

W



MATCH LINE WITH
U ON 5-6

U-1

U

132

FIG. 6-2

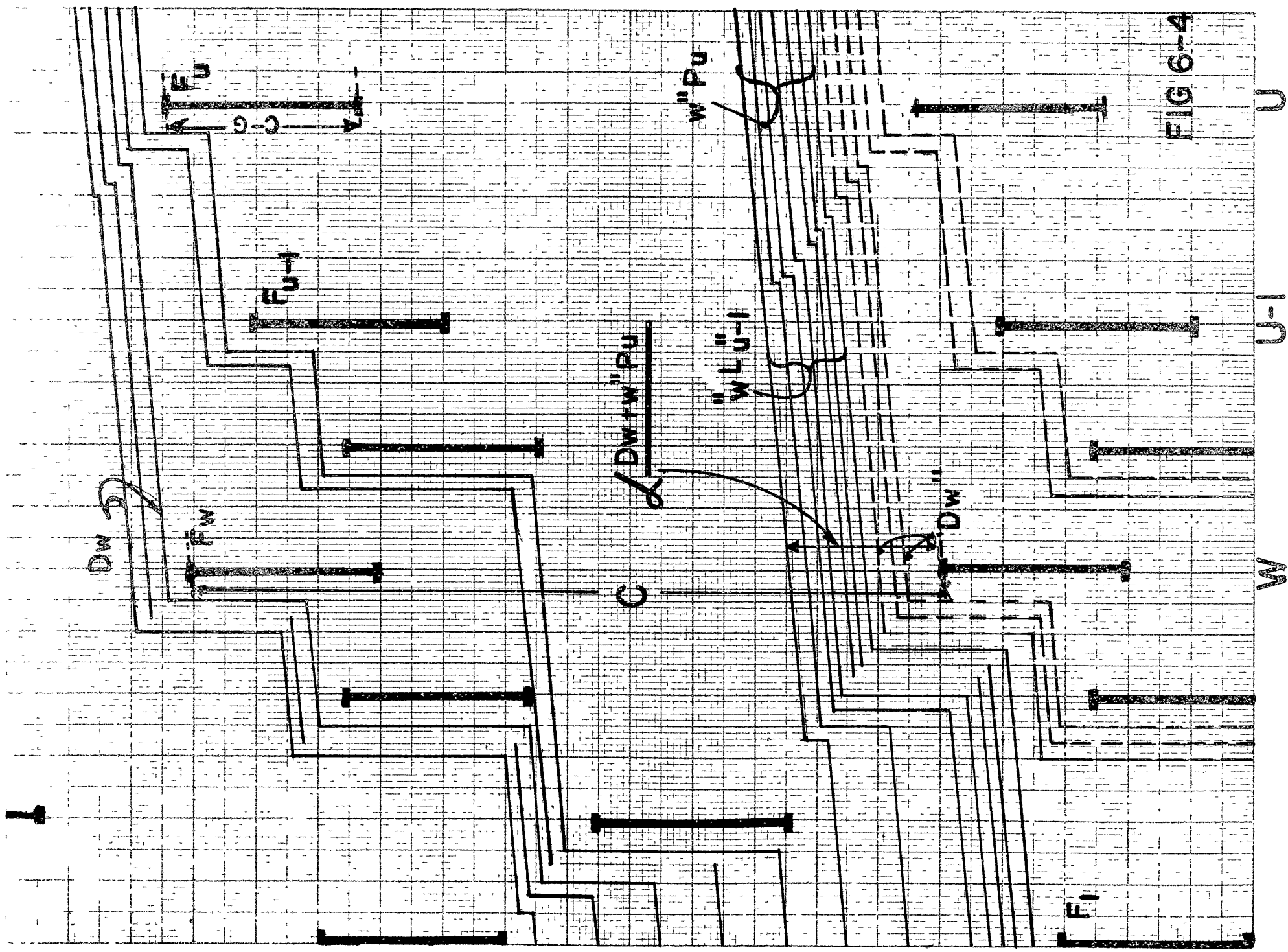



FIG 6-4


 10 X 10 FT 1/4 IN. H 46 1472
 7/8 X 10 IN. MADE IN U.S.A.
 YEUTFEI 11-4111 CO

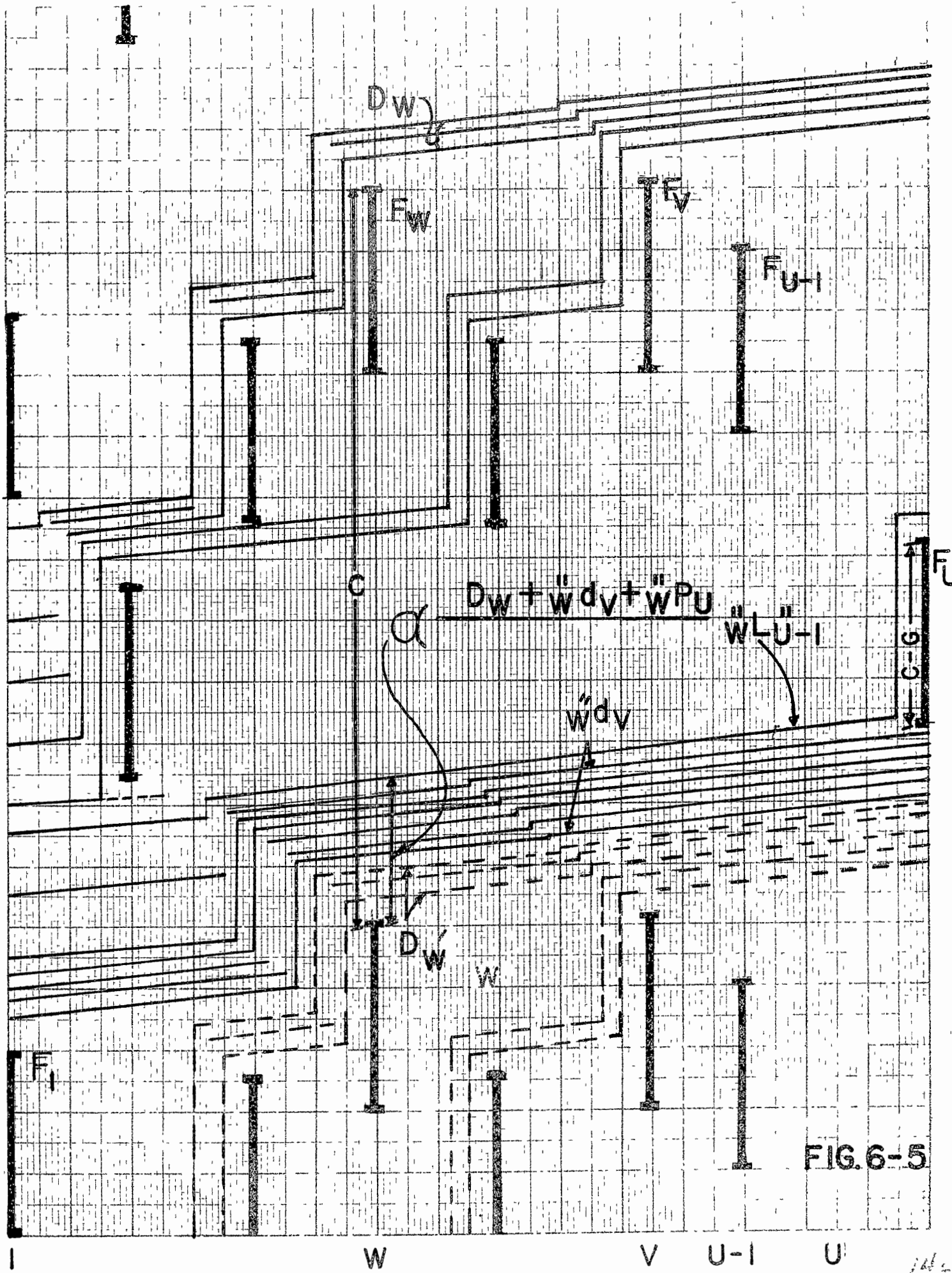


FIG. 6-5

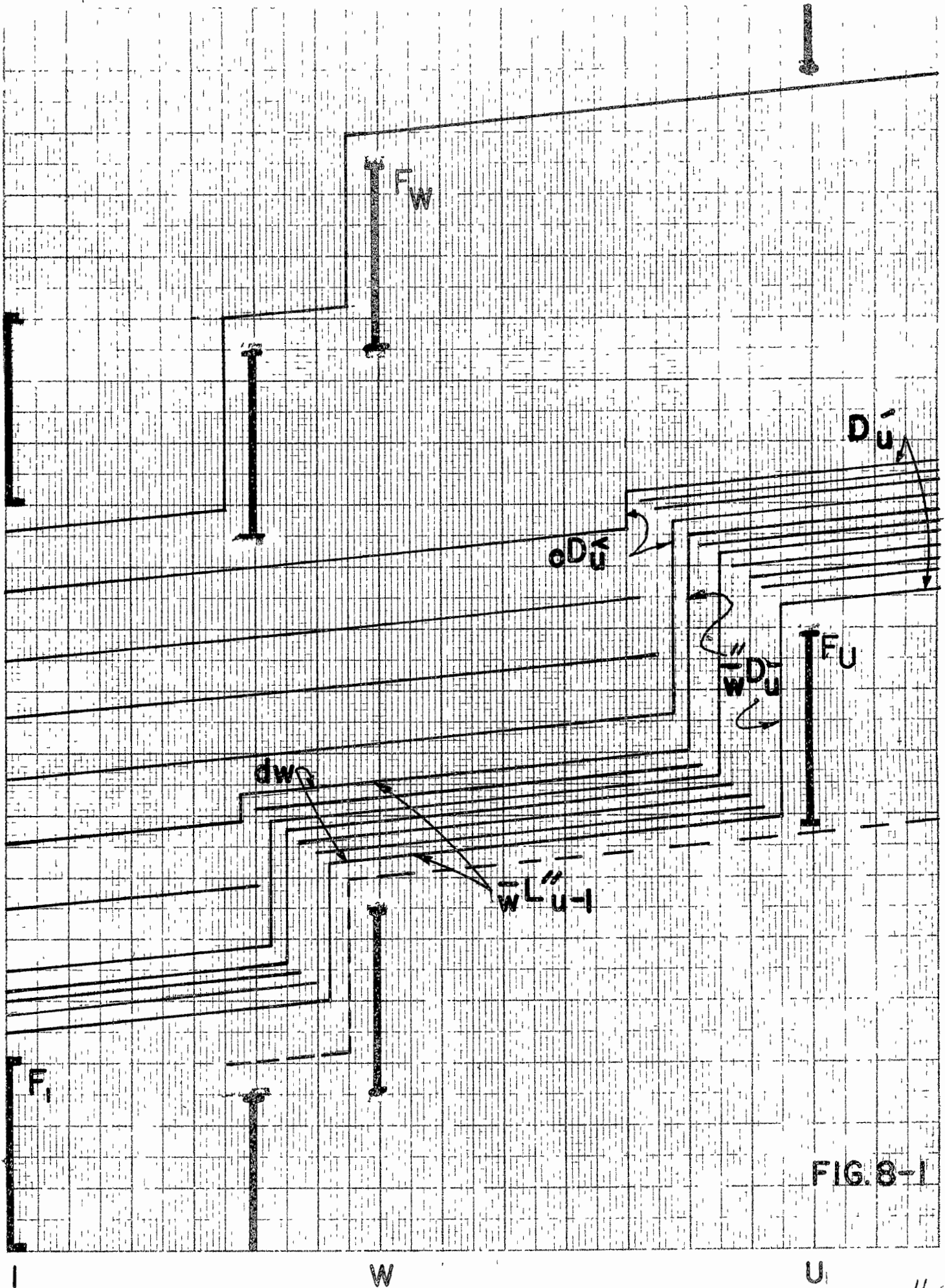


FIG. 8-1

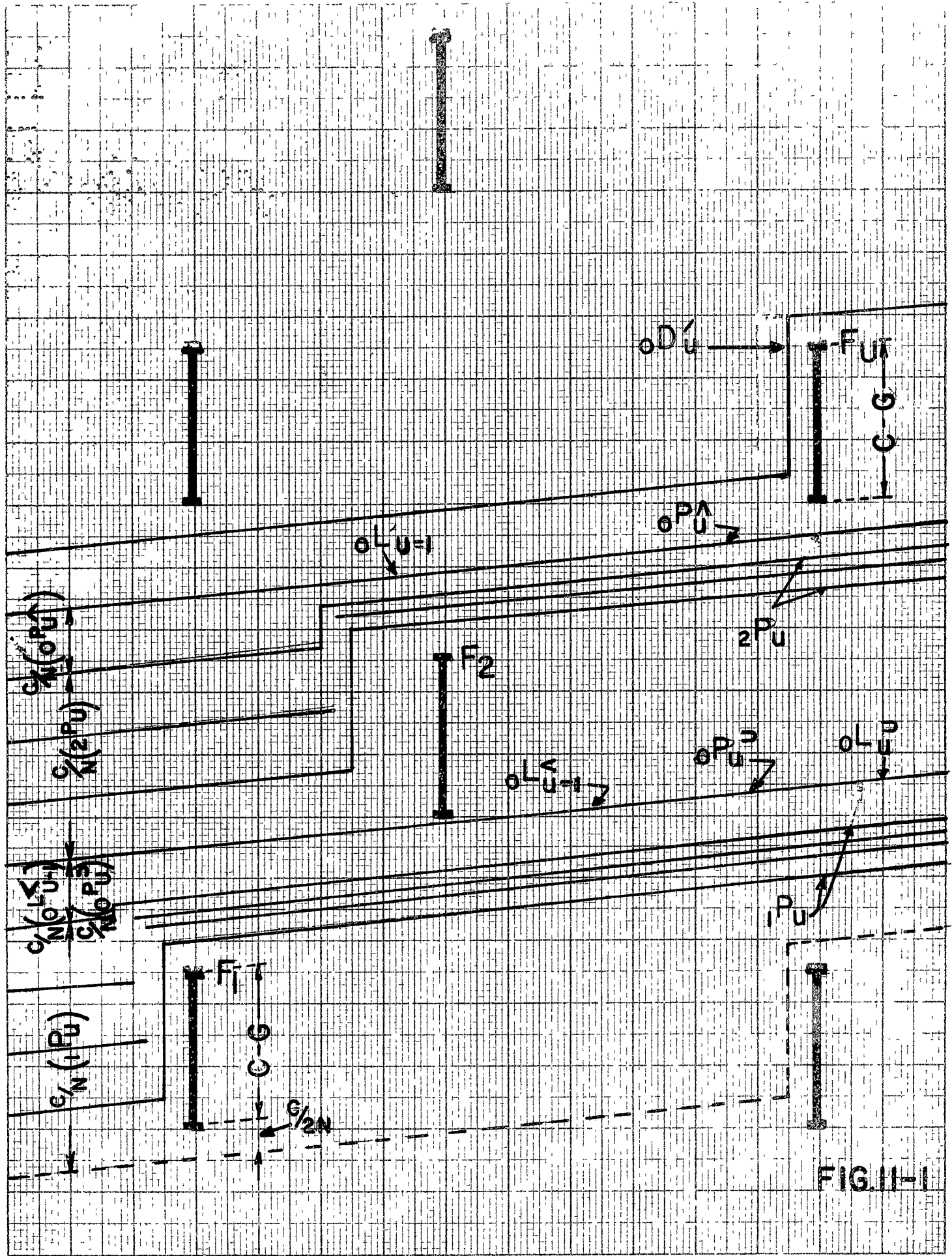
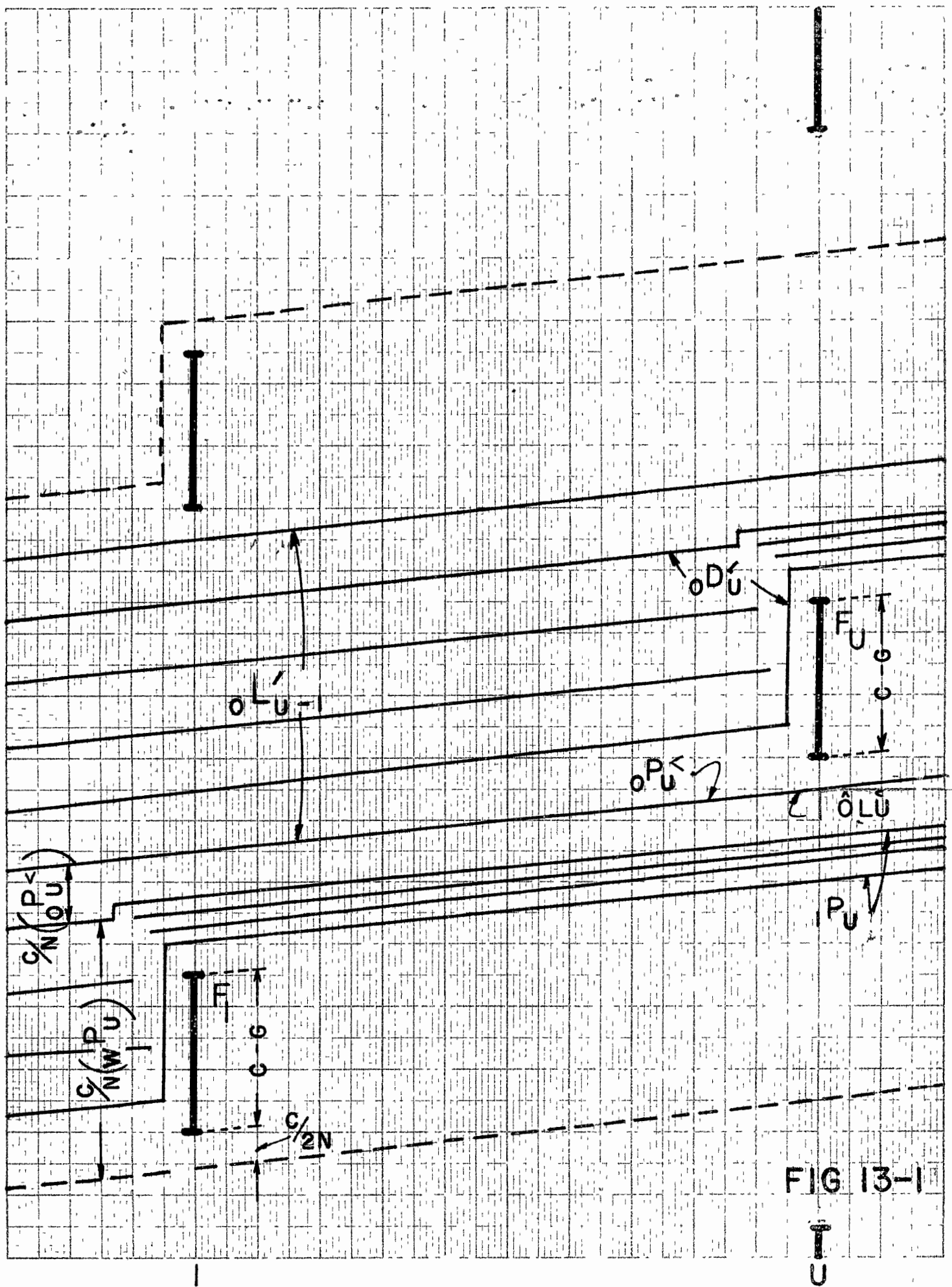


FIG. II-1



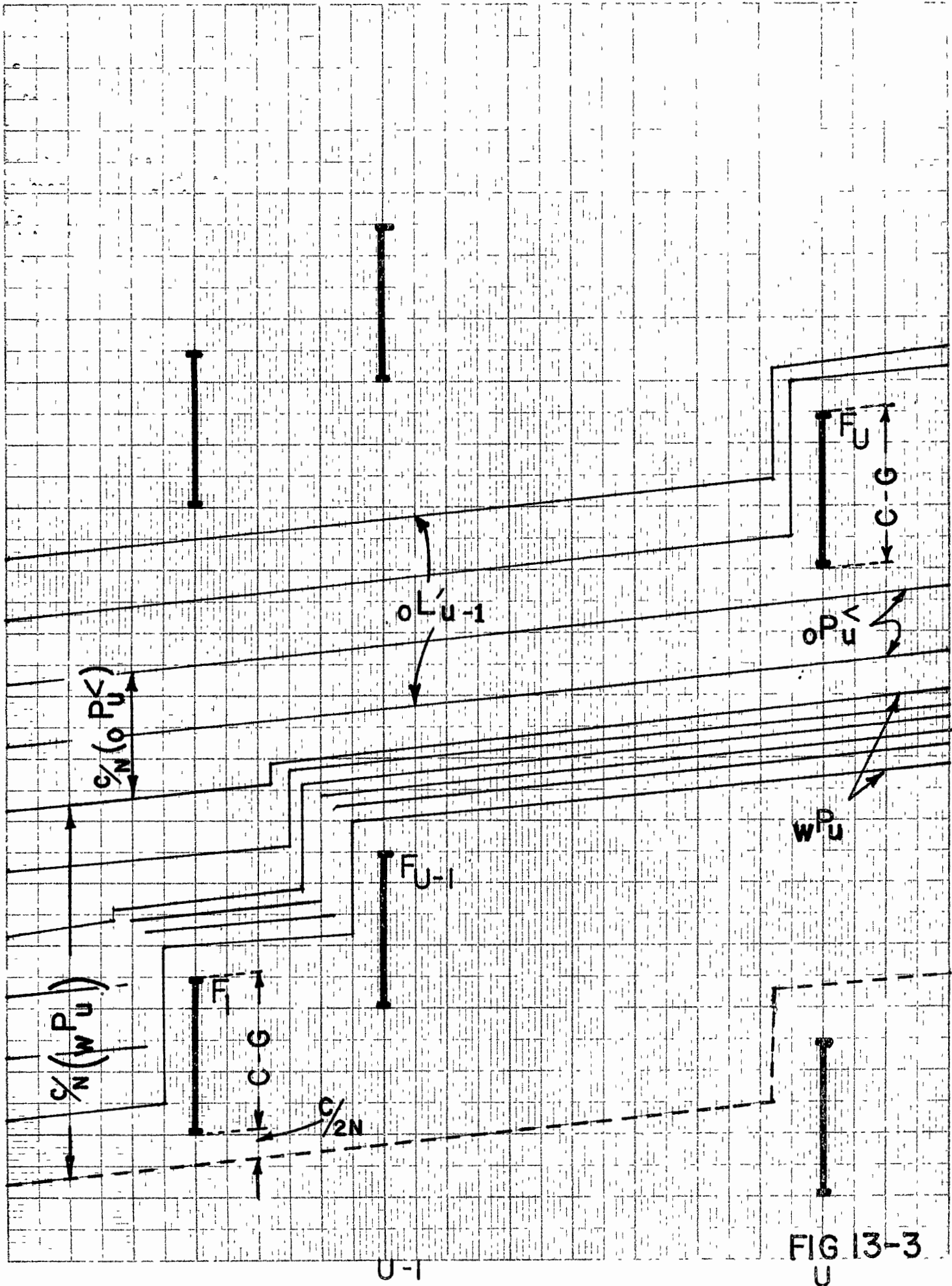


FIG 13-3
U

12 x 10 1/2 INCH 46 1470
 N. E. W. 10 CMIS
 SUPPLY CO.

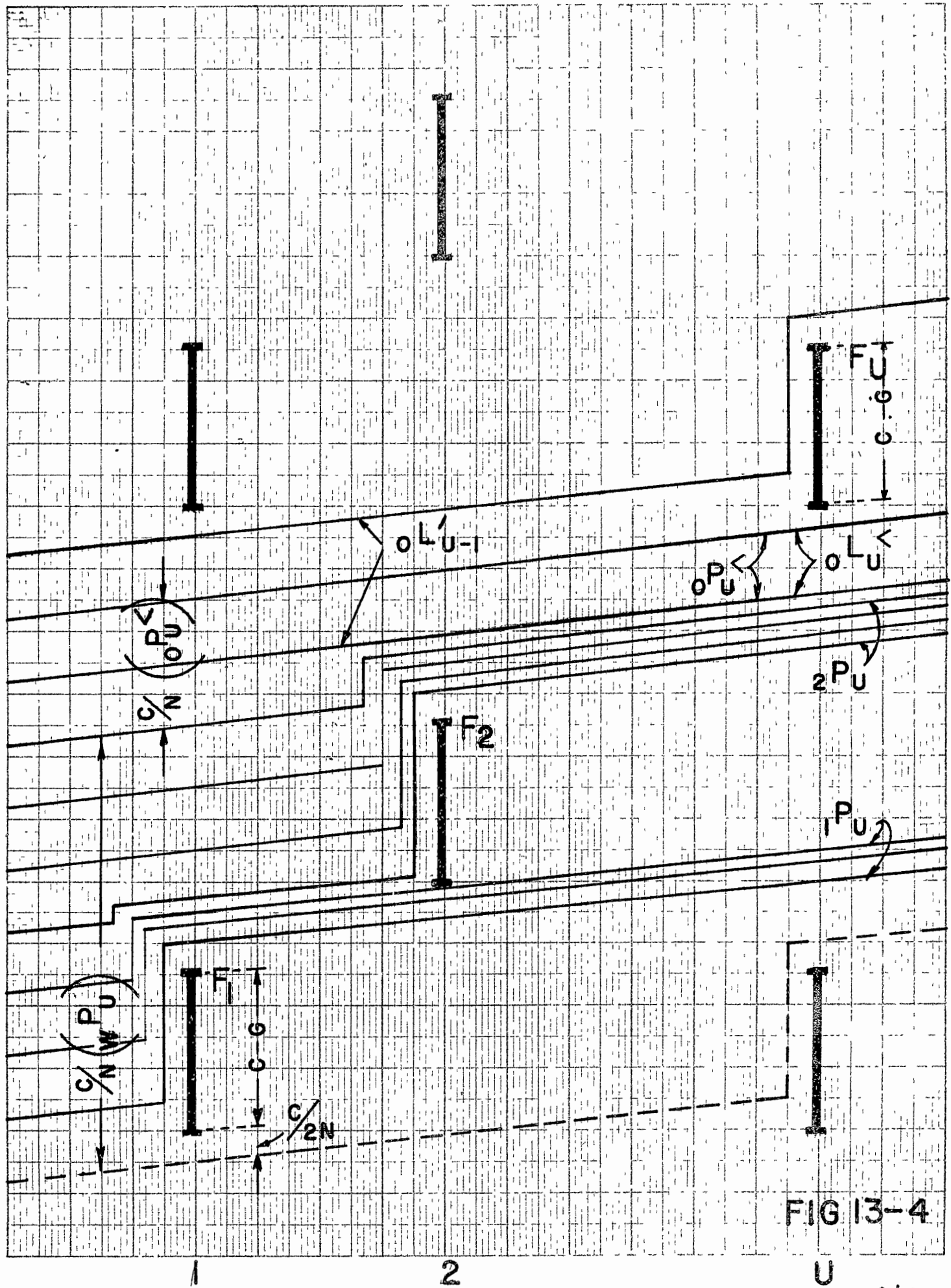


FIG 13-4

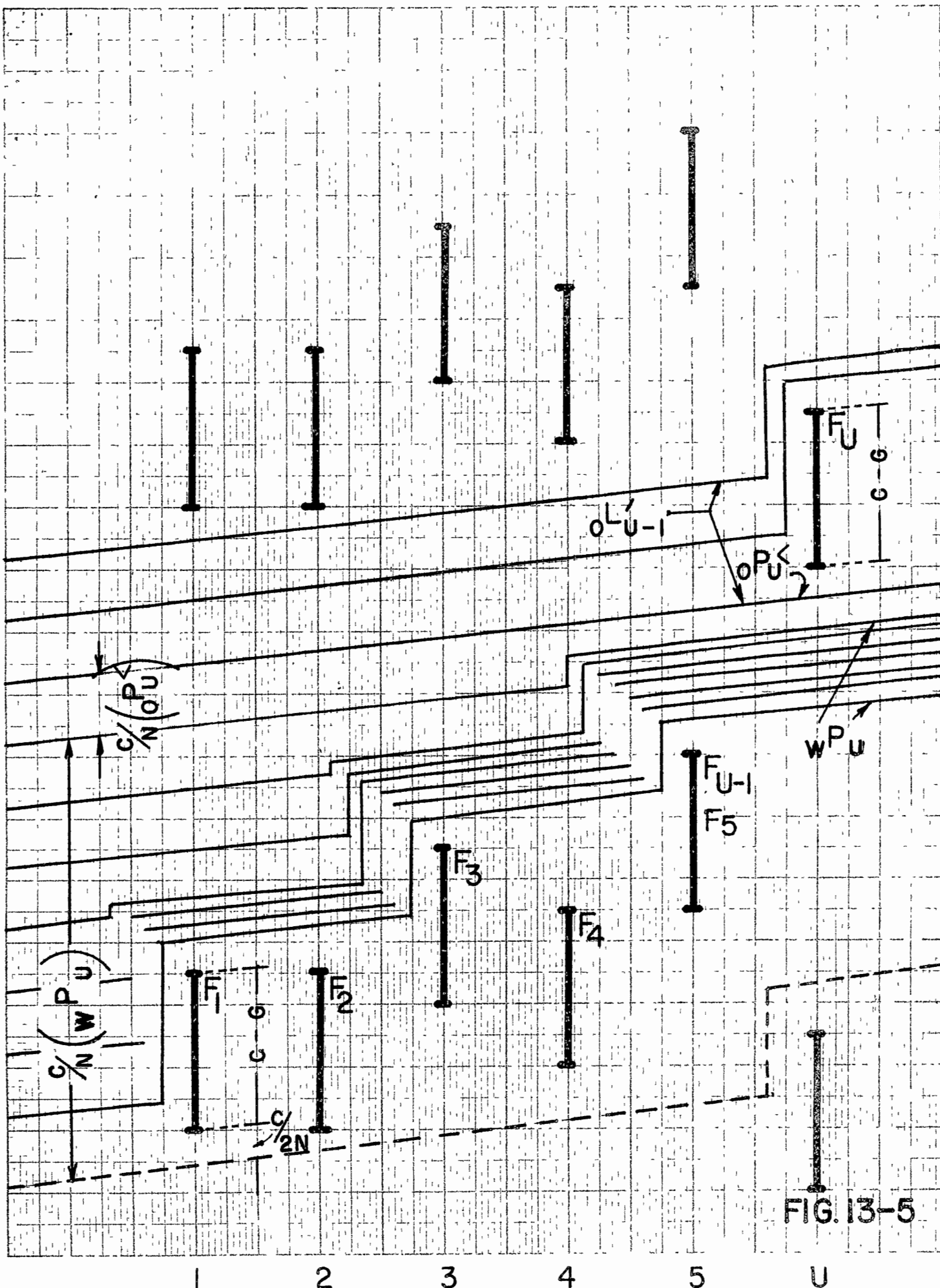


FIG. 13-5

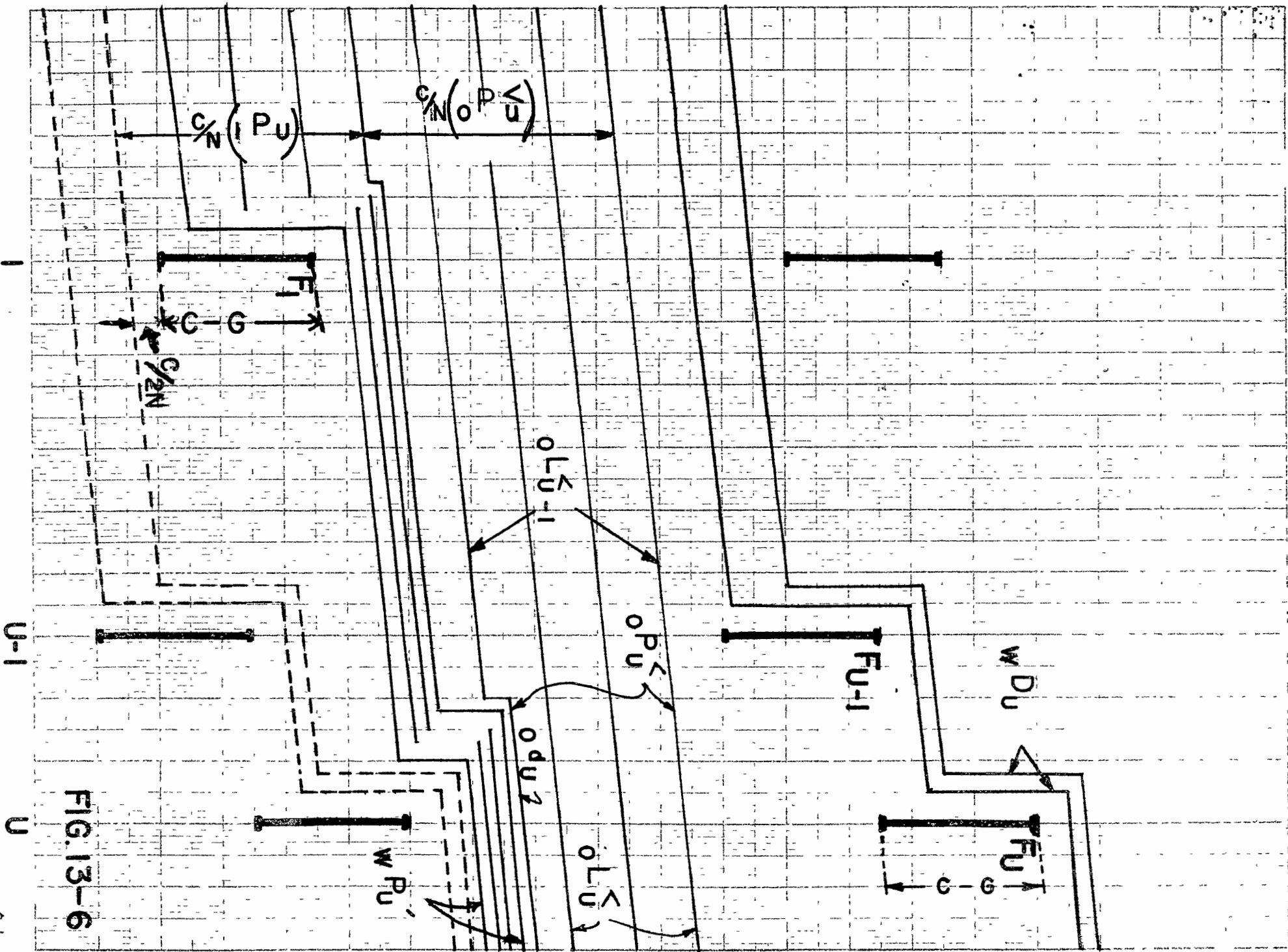


FIG. 13-6

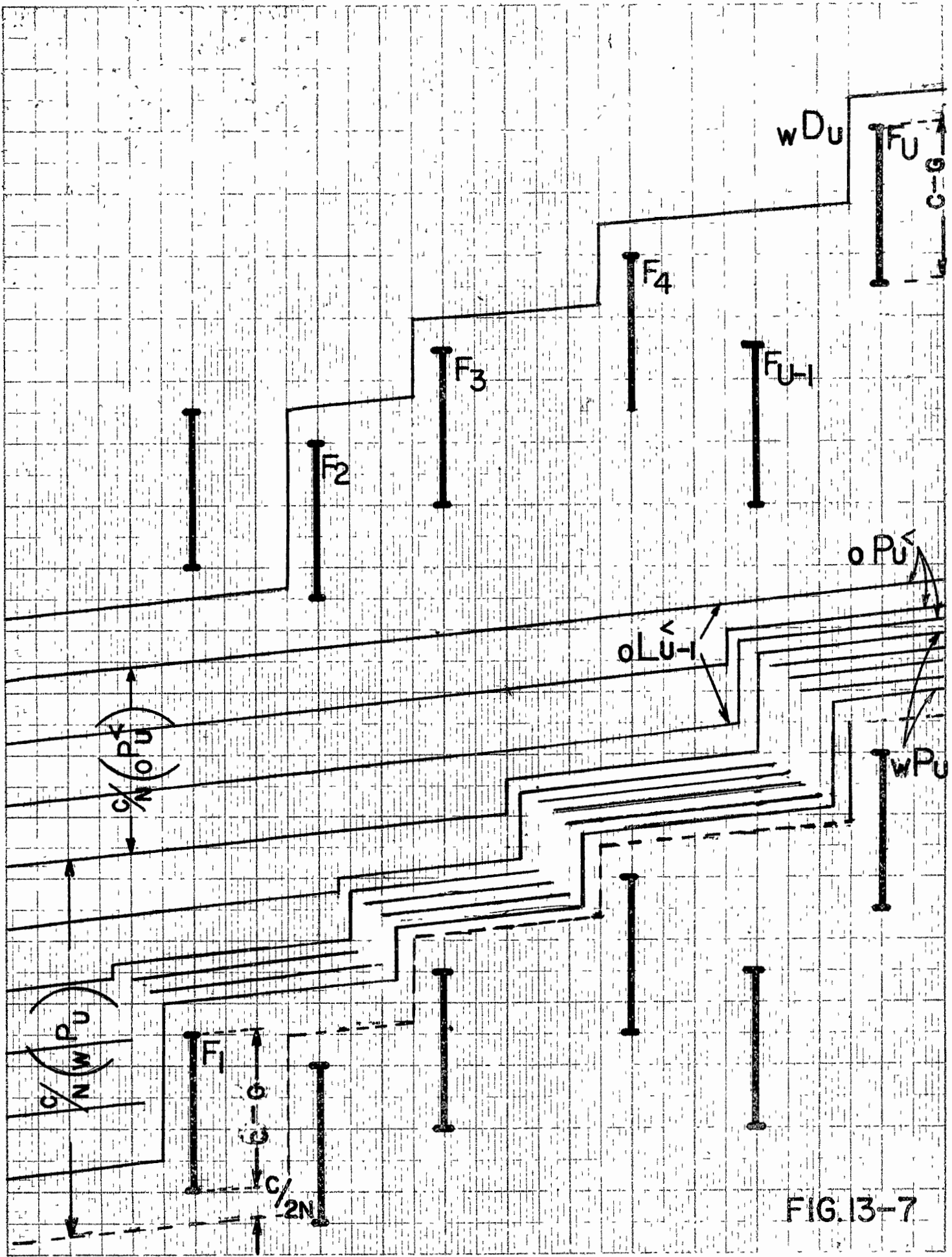


FIG. 13-7

10 X 10 TO 1 1/2 INCH 46 1470
 X 10 IP CHFS
 KUFFEL / ESSEL CO

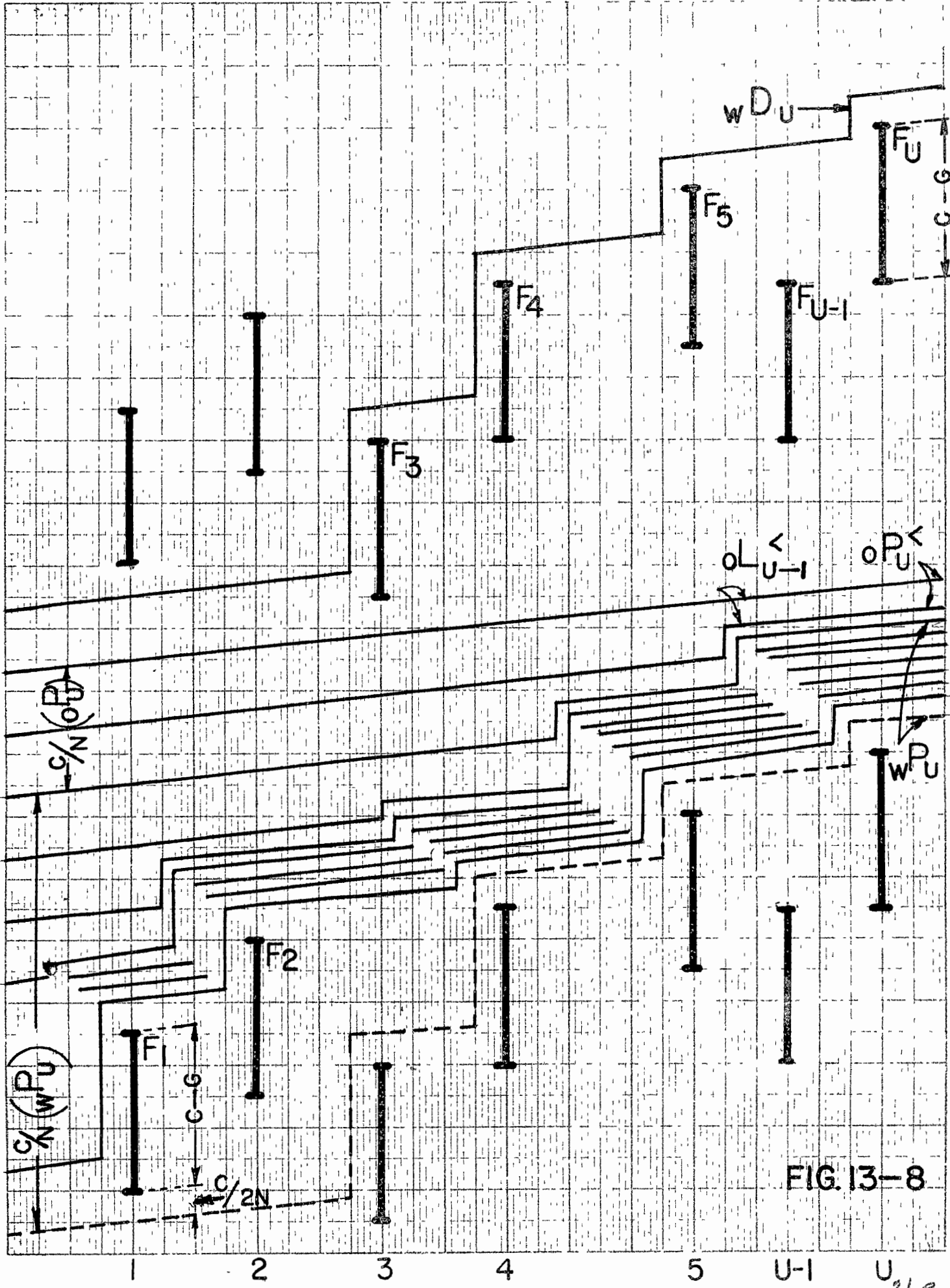


FIG. 13-8

2/e

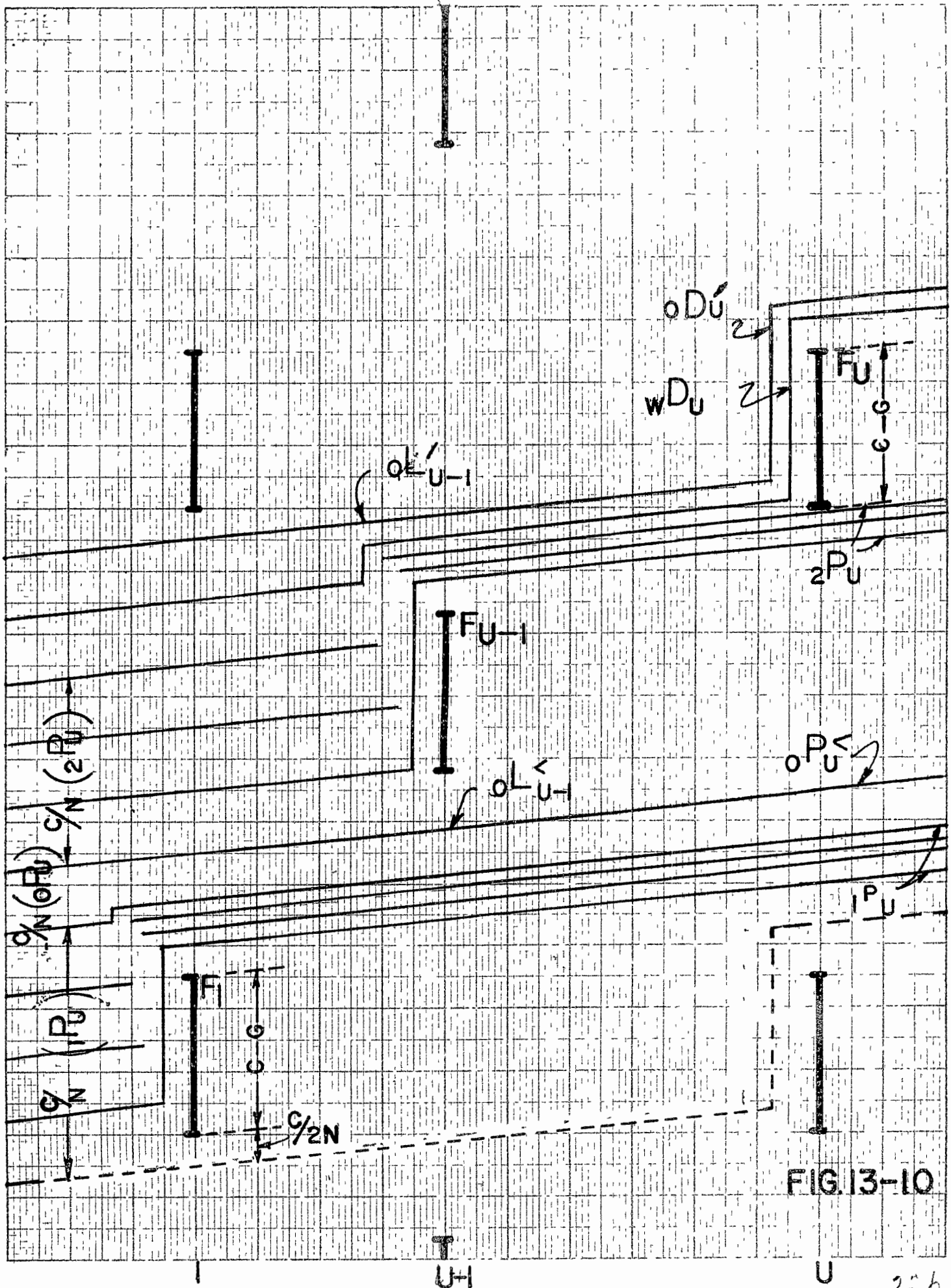


FIG. 13-10

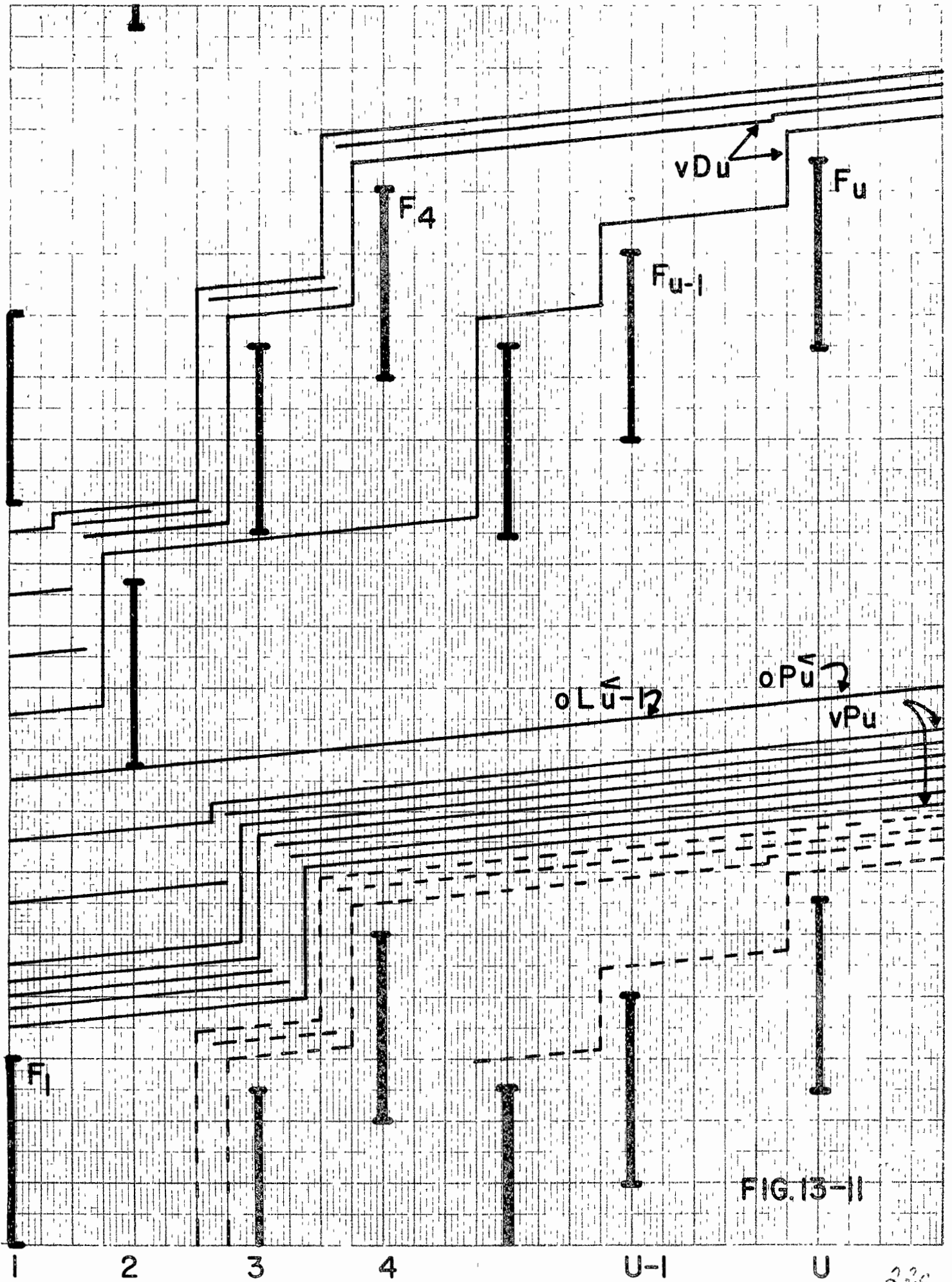


FIG.13-II

10 X 10 TO 13 INCH 40 11/20
7/8 X 1/2 UNES
K
VEN.FEE. 05511 C

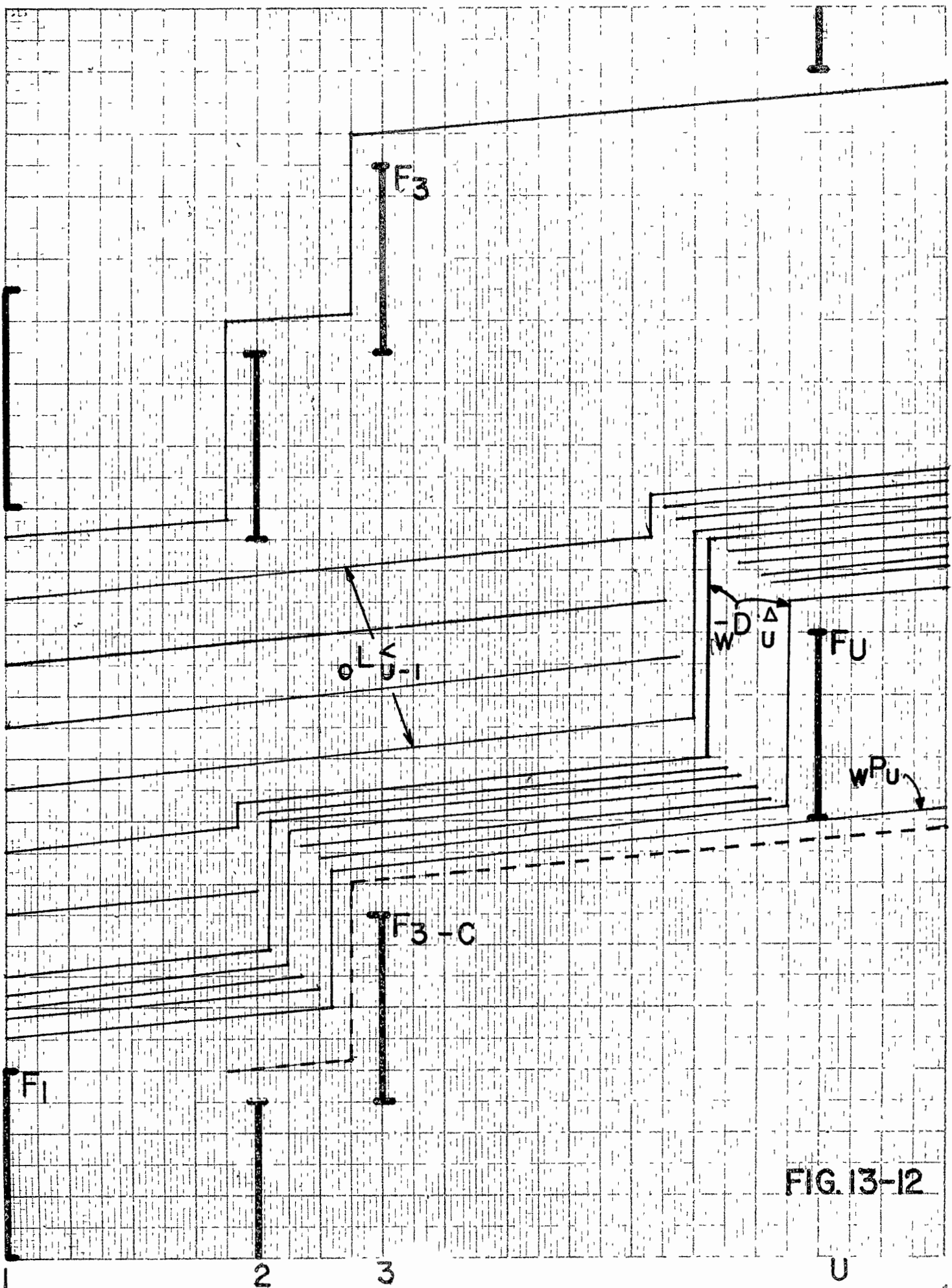


FIG. 13-12

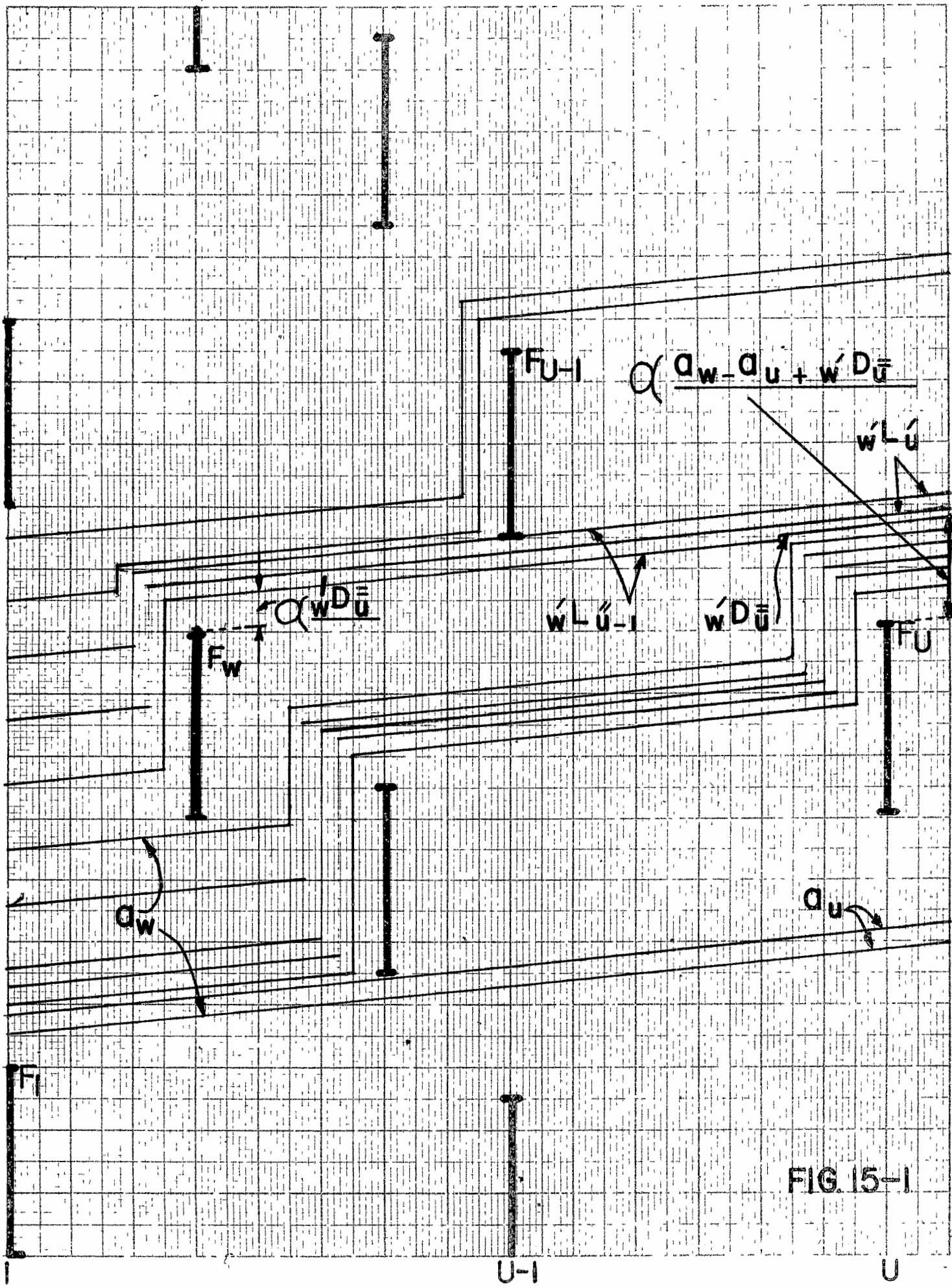


FIG. 15-1

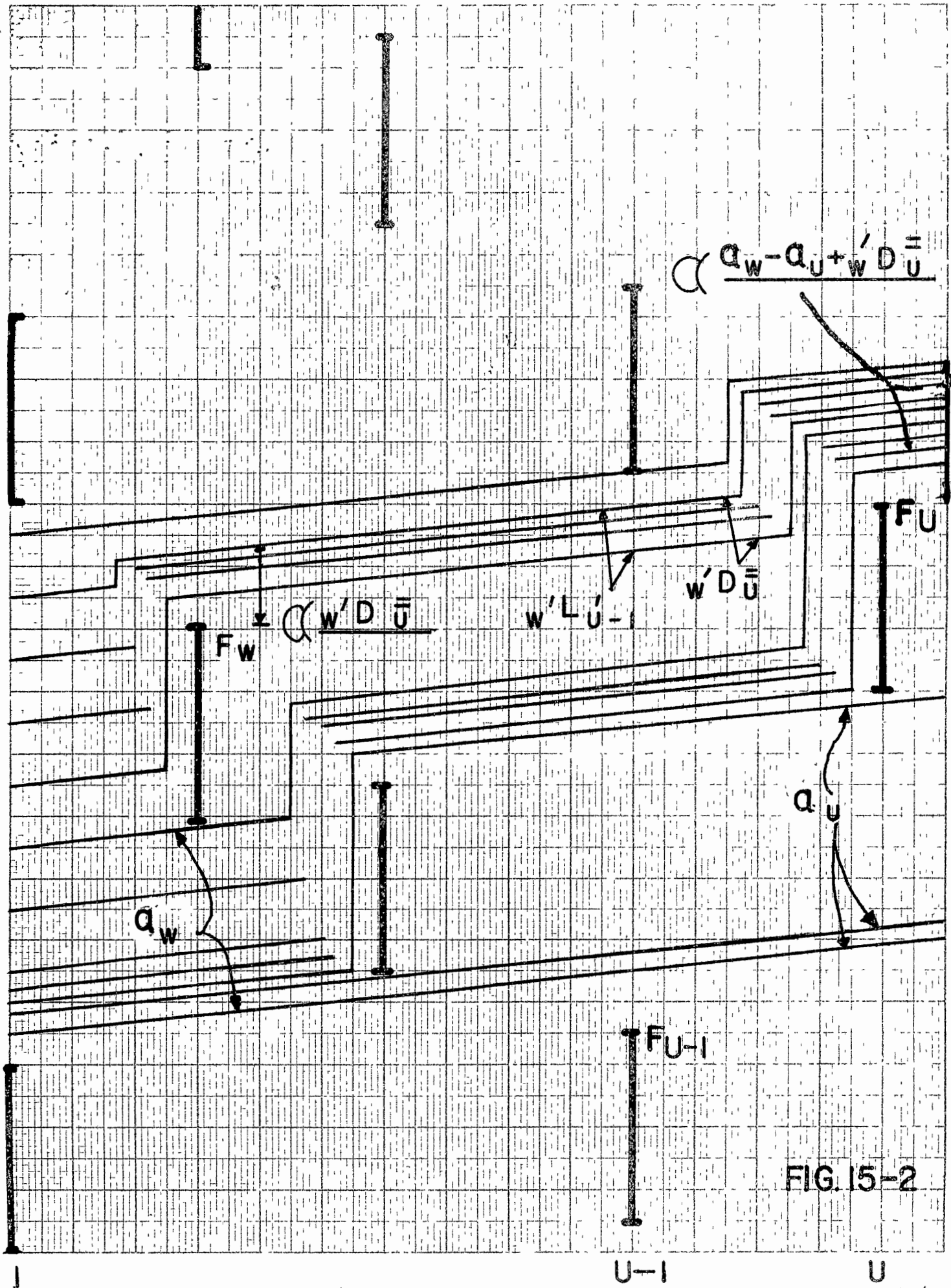


FIG. 15-2

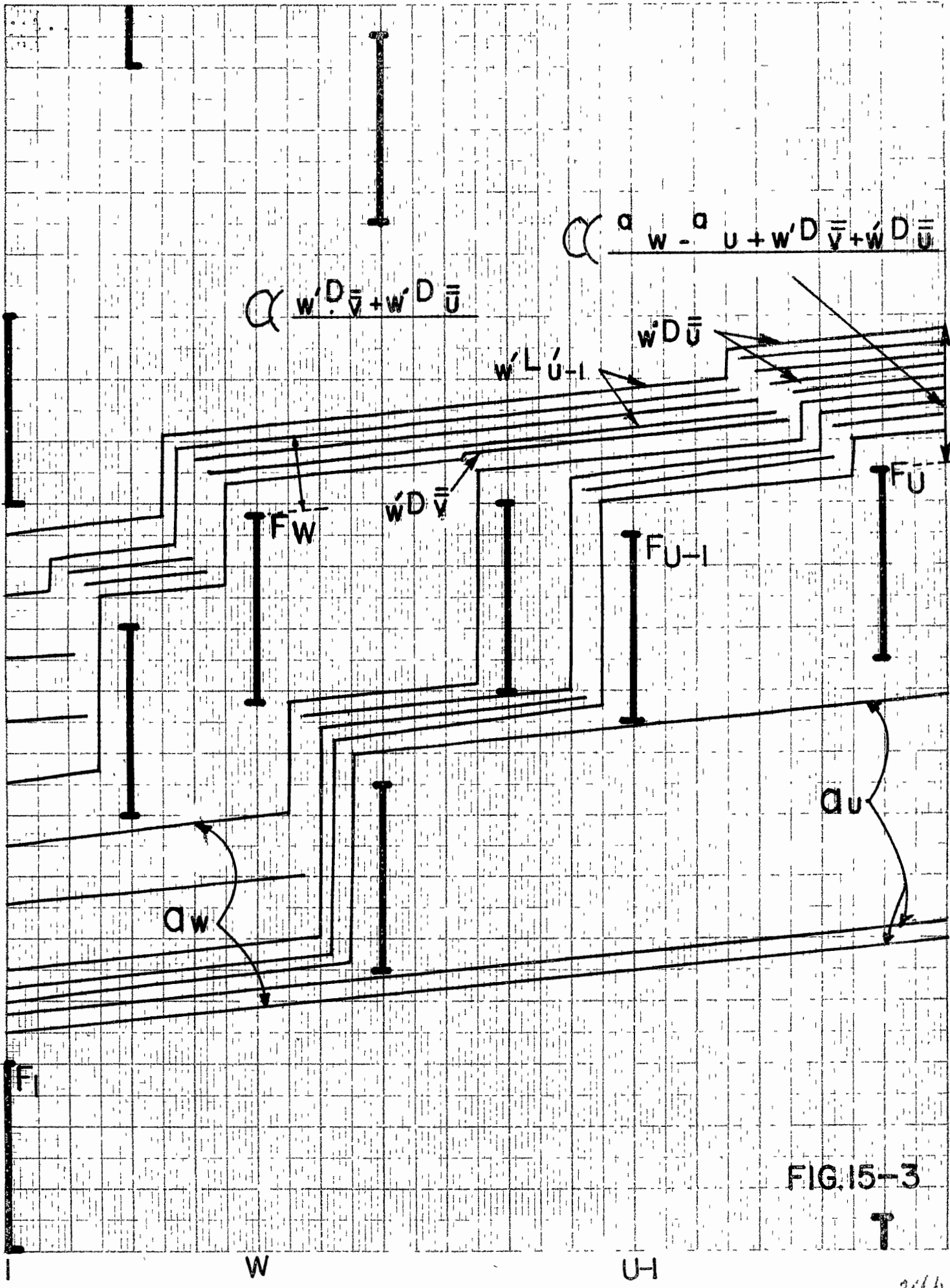


FIG.15-3

10 x 10 1/2 INCH 46 1470
 1/4 x 1/4 INCHES V.C.B.S.
 NEUFELI & T.P. CO

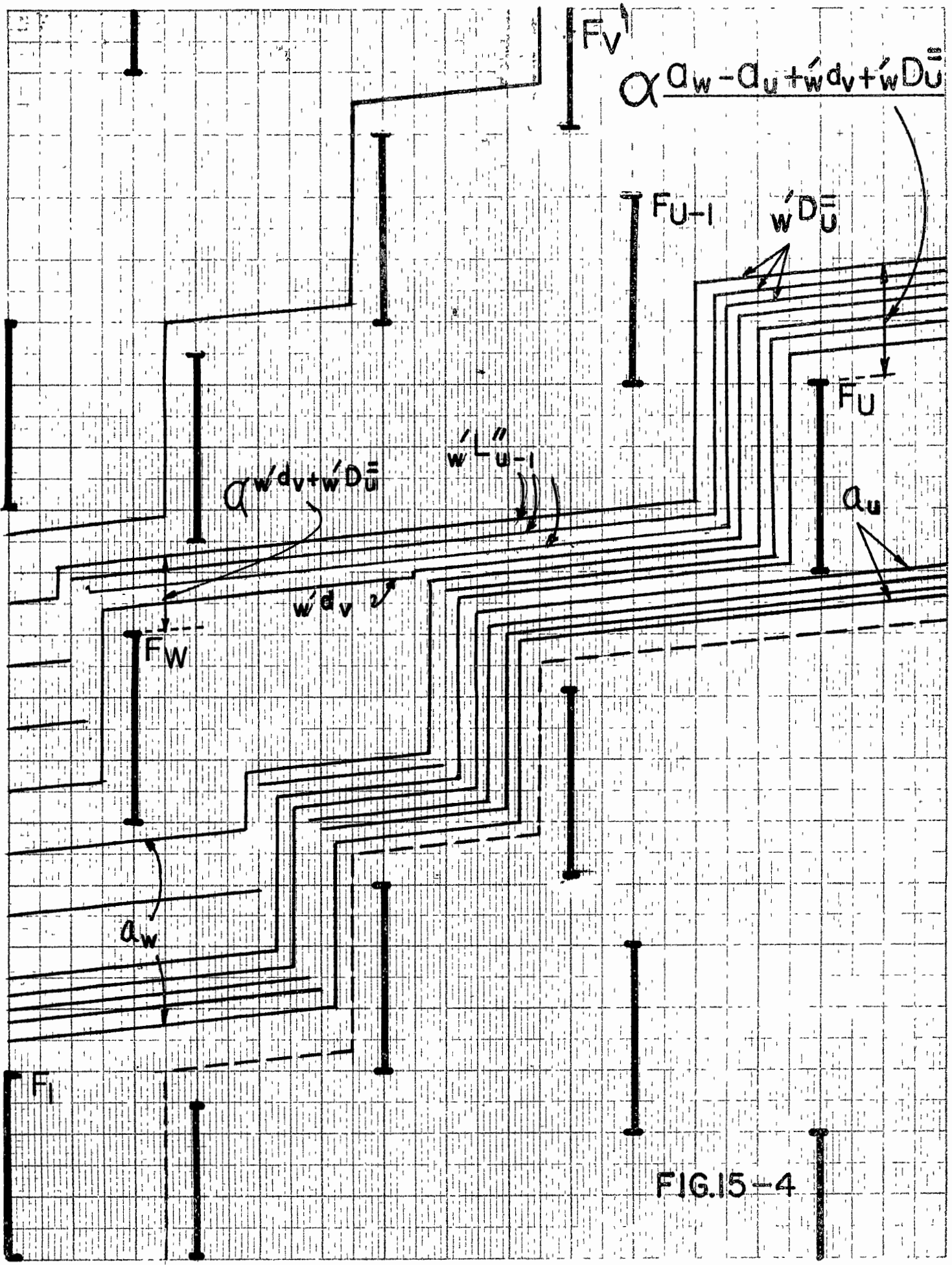


FIG.15-4

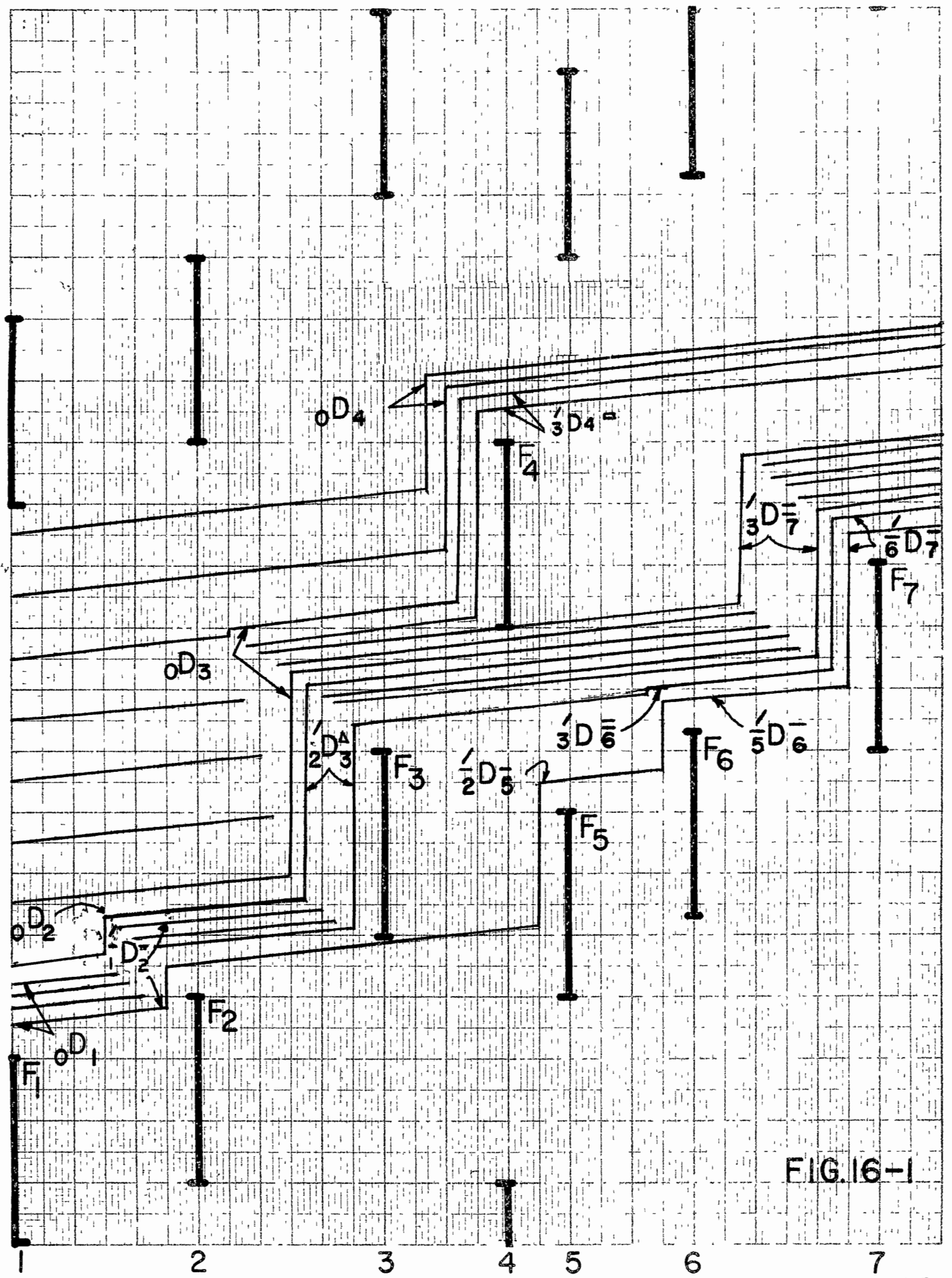


FIG. 16-1

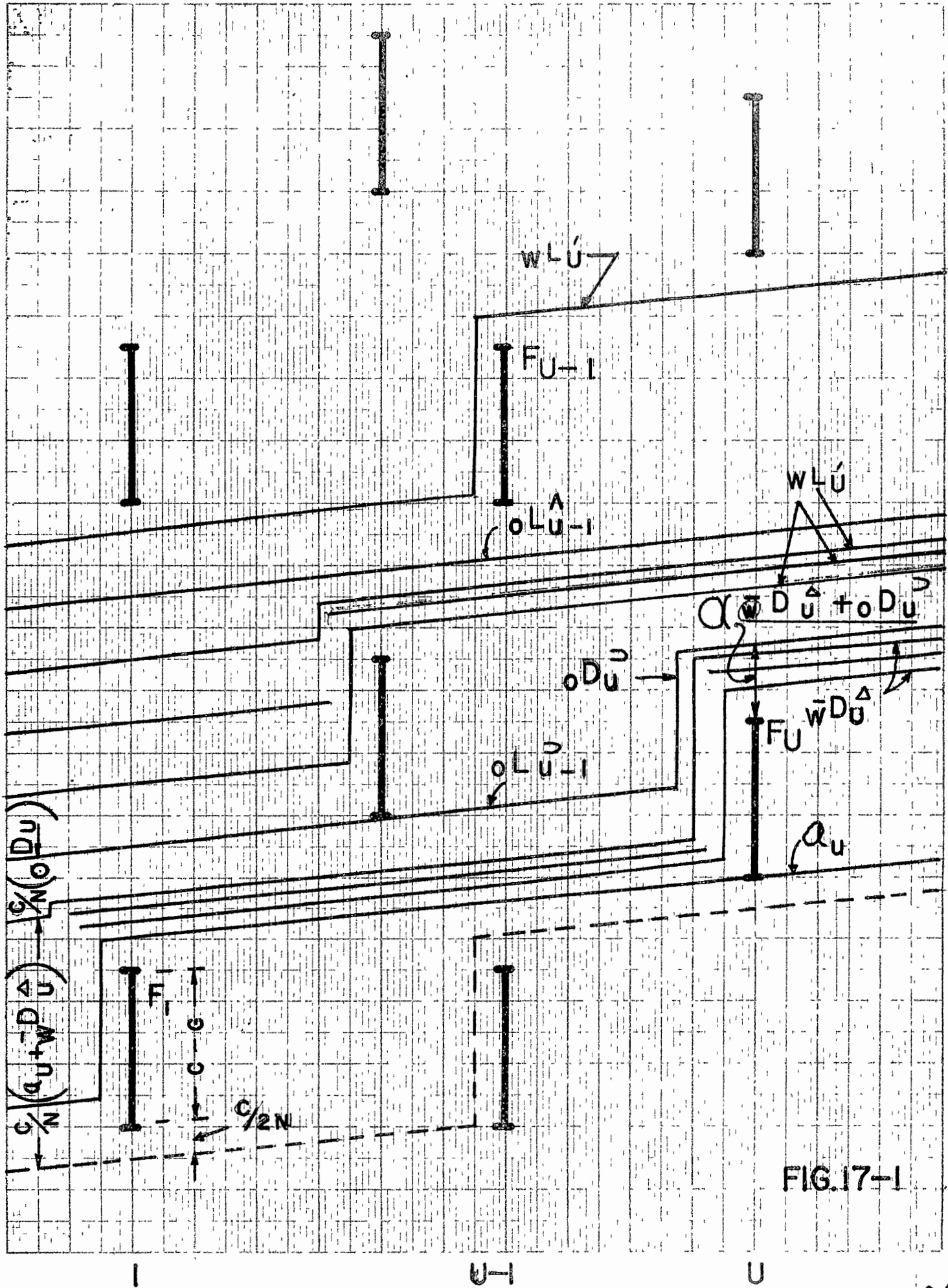


FIG. 17-1

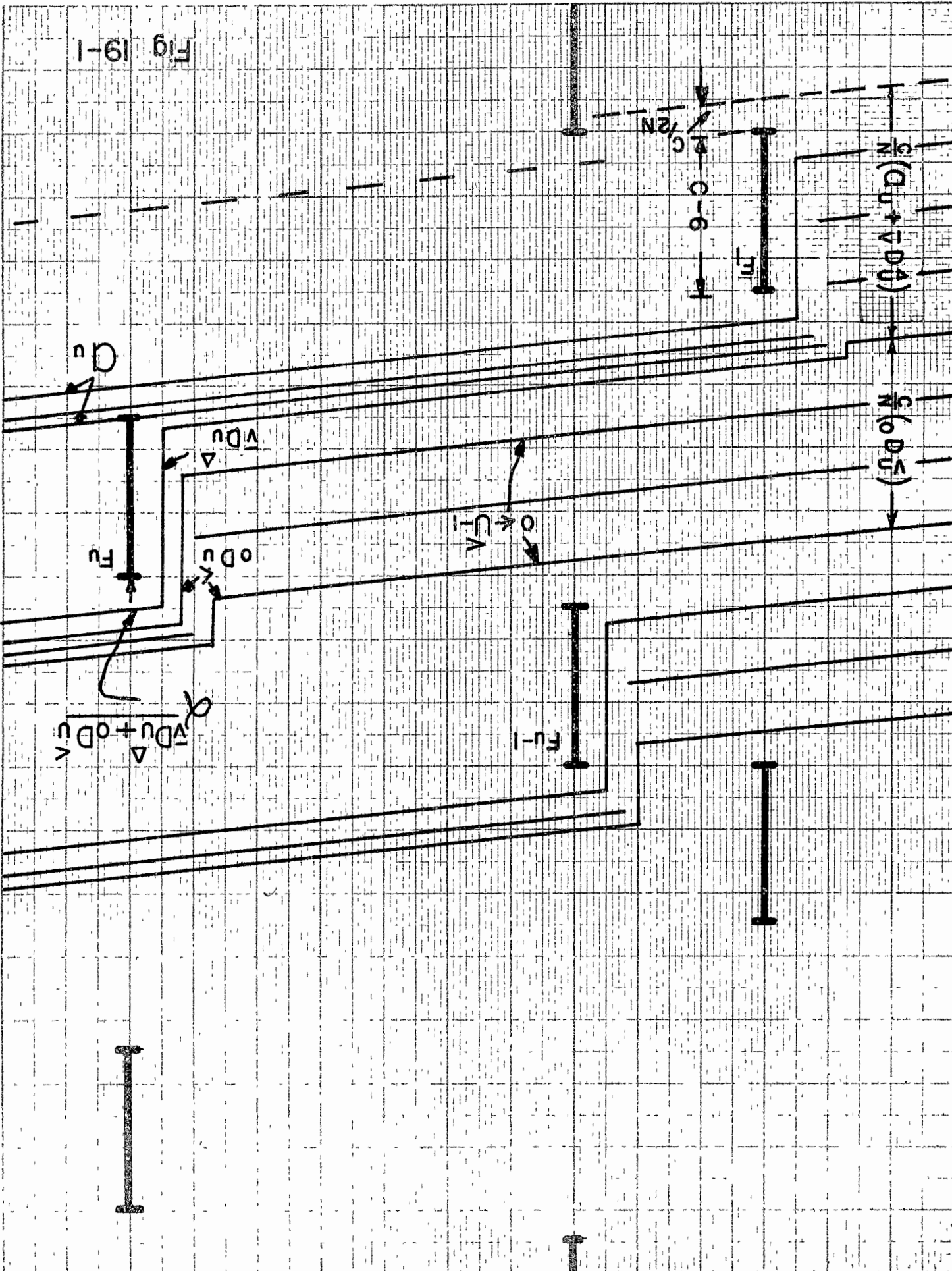


Fig 19-1

27

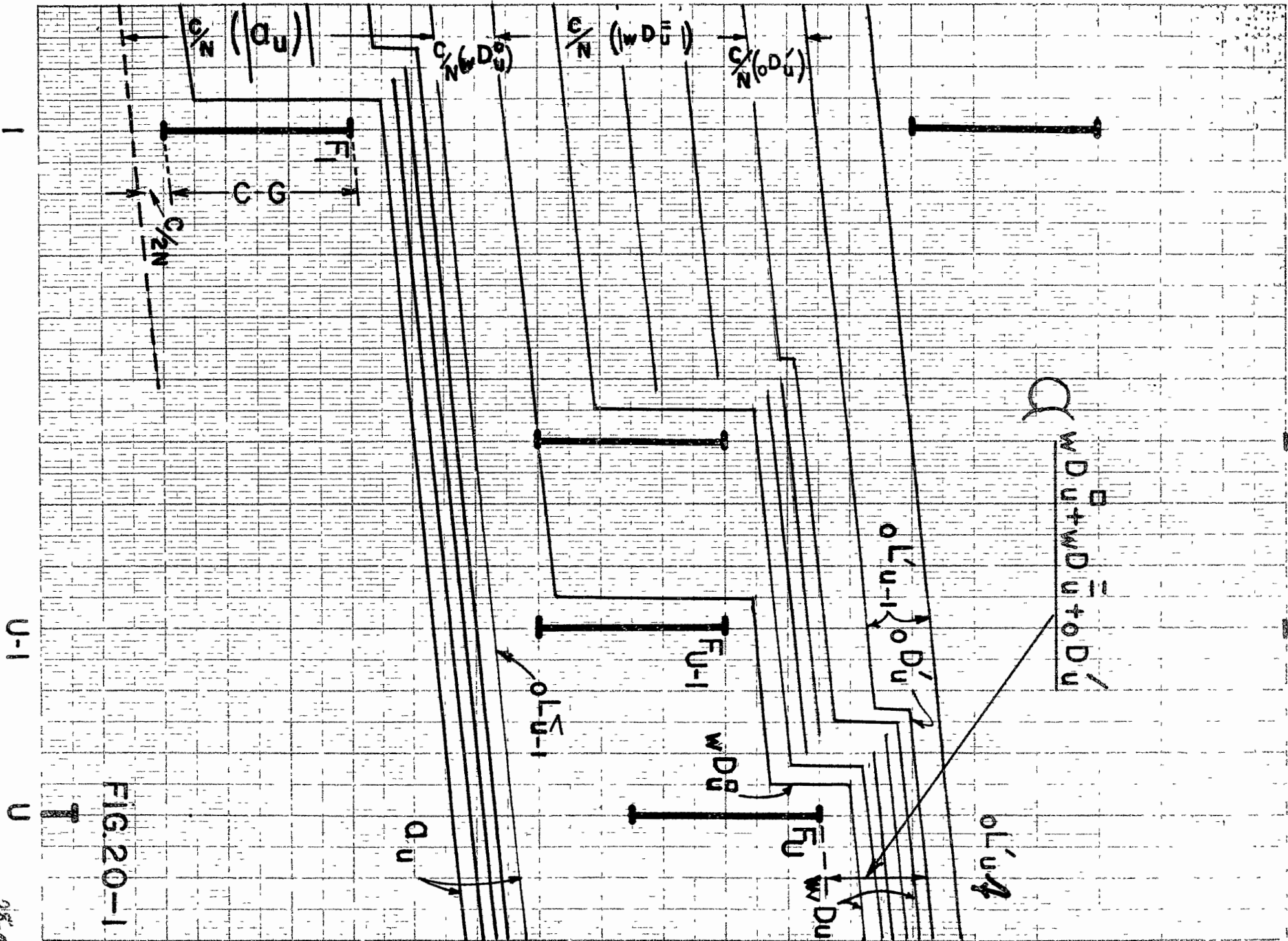


FIG. 20-1

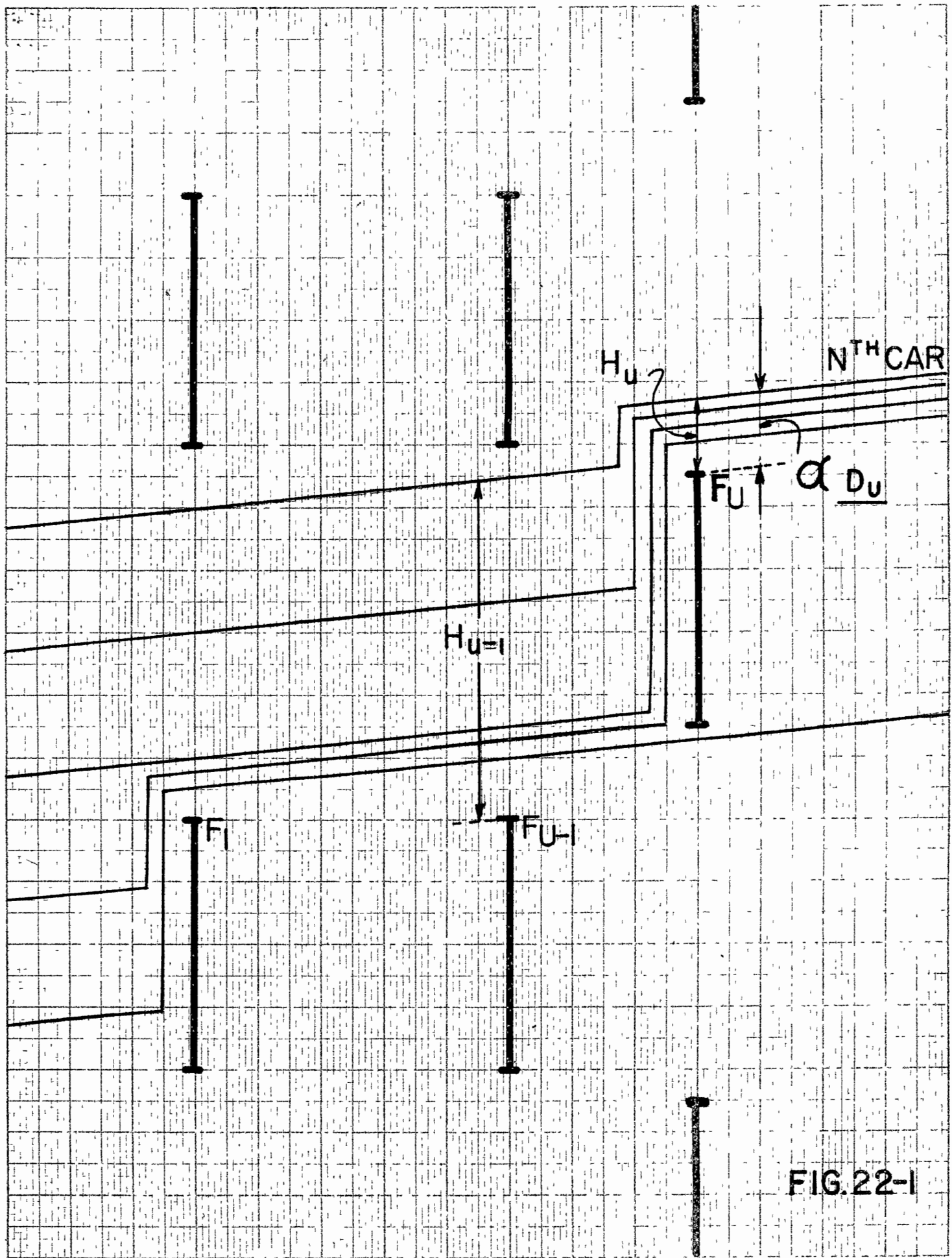


FIG. 22-1

REF ID: A61147C
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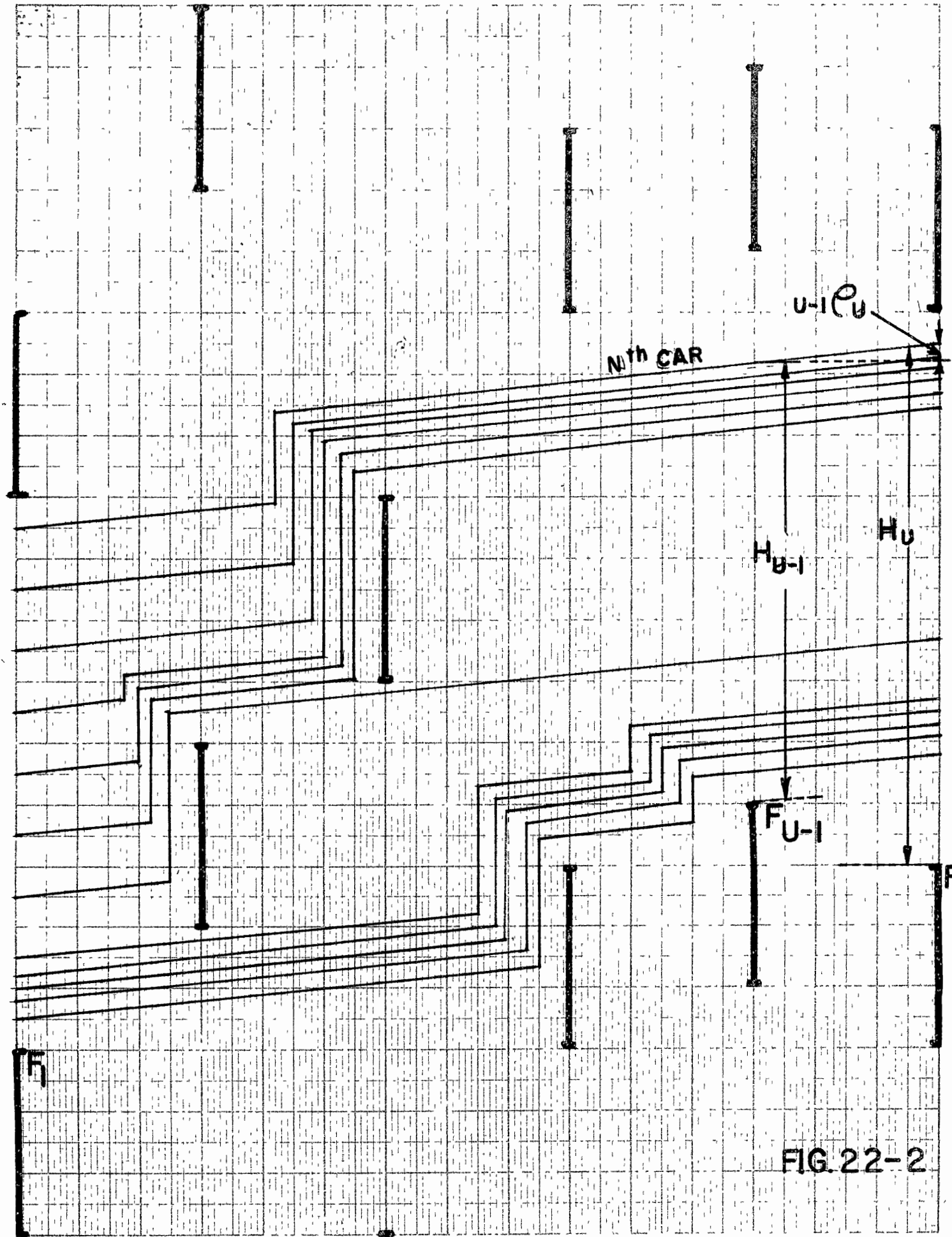


FIG. 22-2

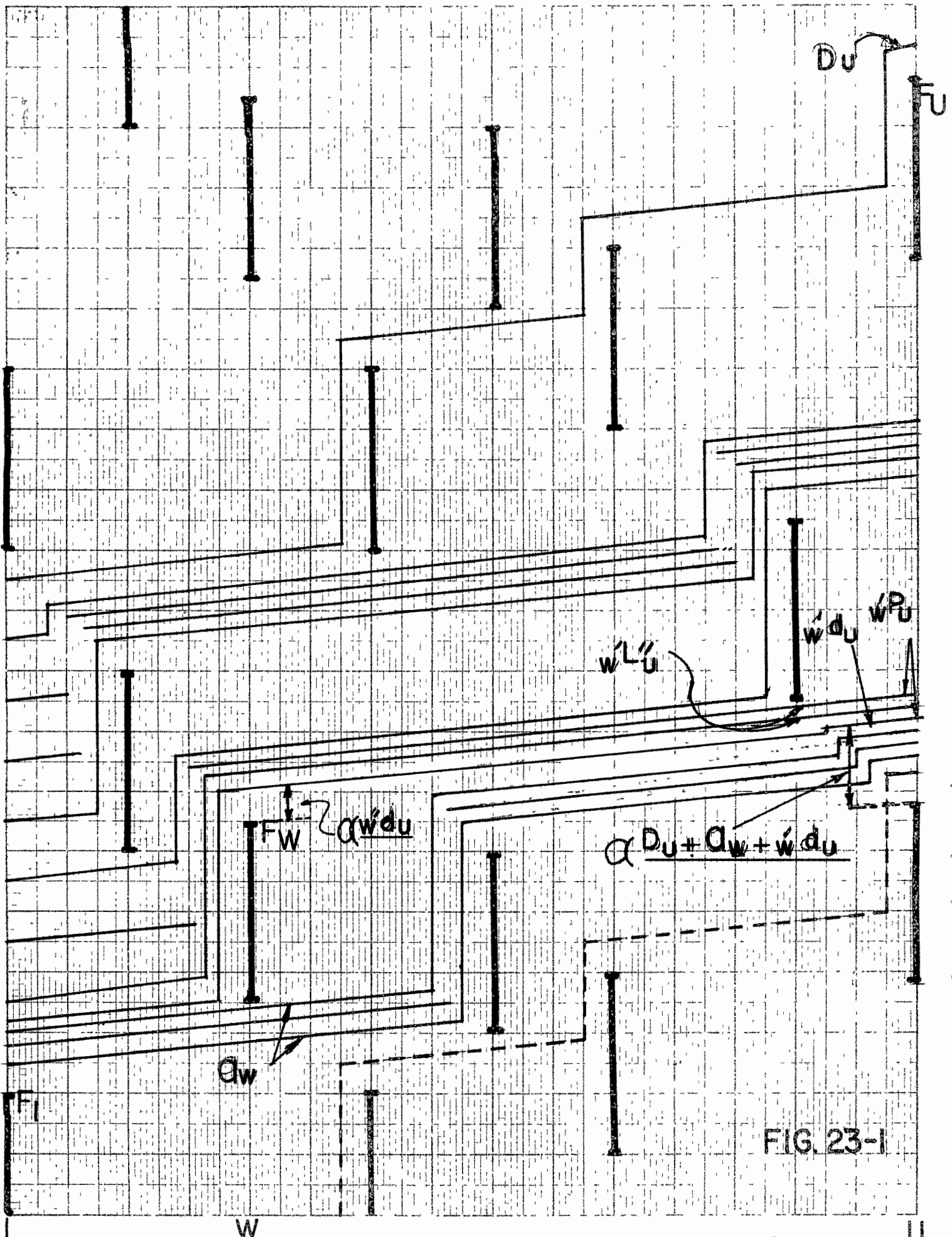


FIG. 23-1

10 X 10 TO 1 1/2 INCH 46 1470
 7 1/2 X 10 HIGHS 470L II 57
 KEUF 11 FESER CO

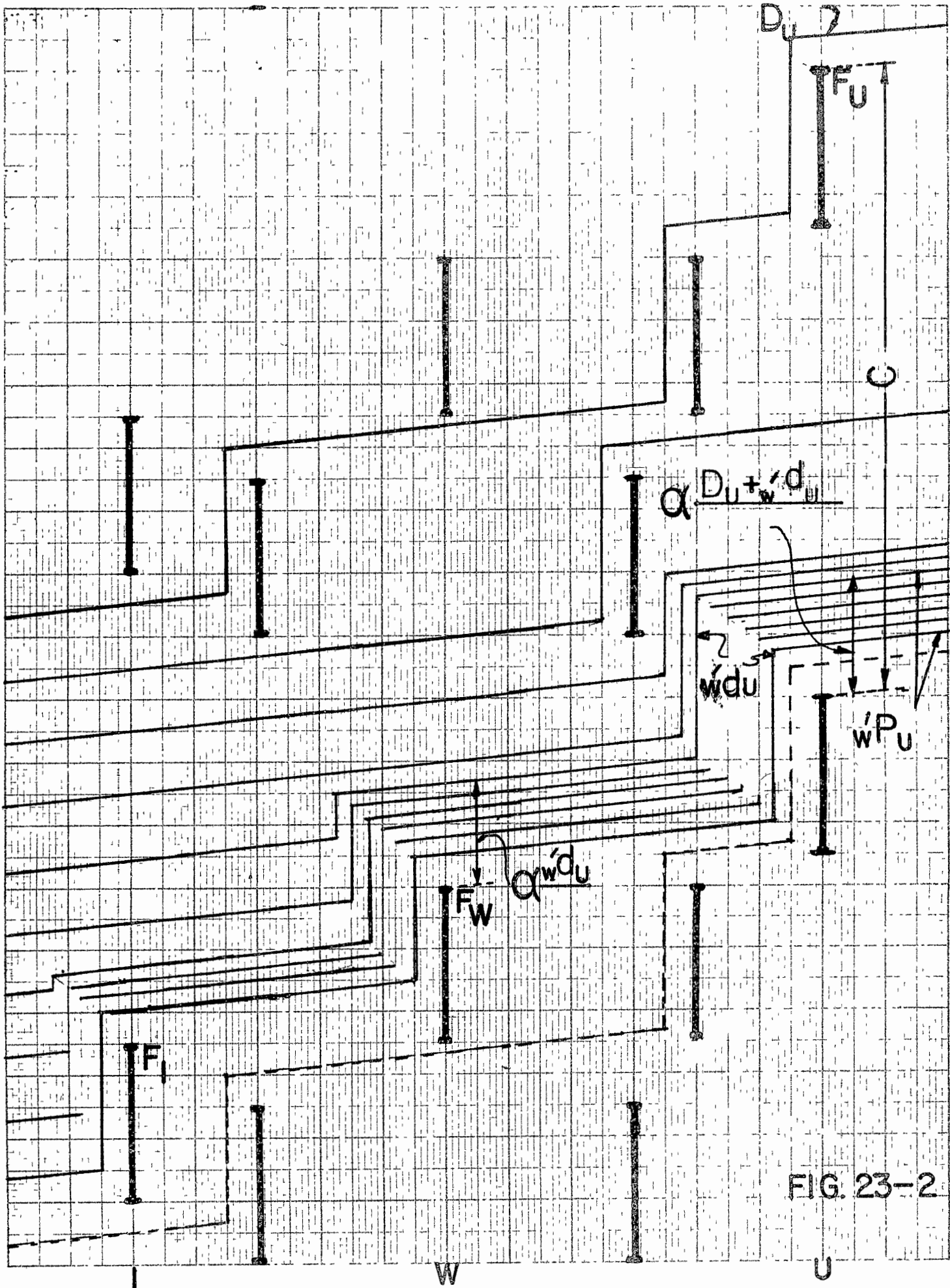


FIG. 23-2

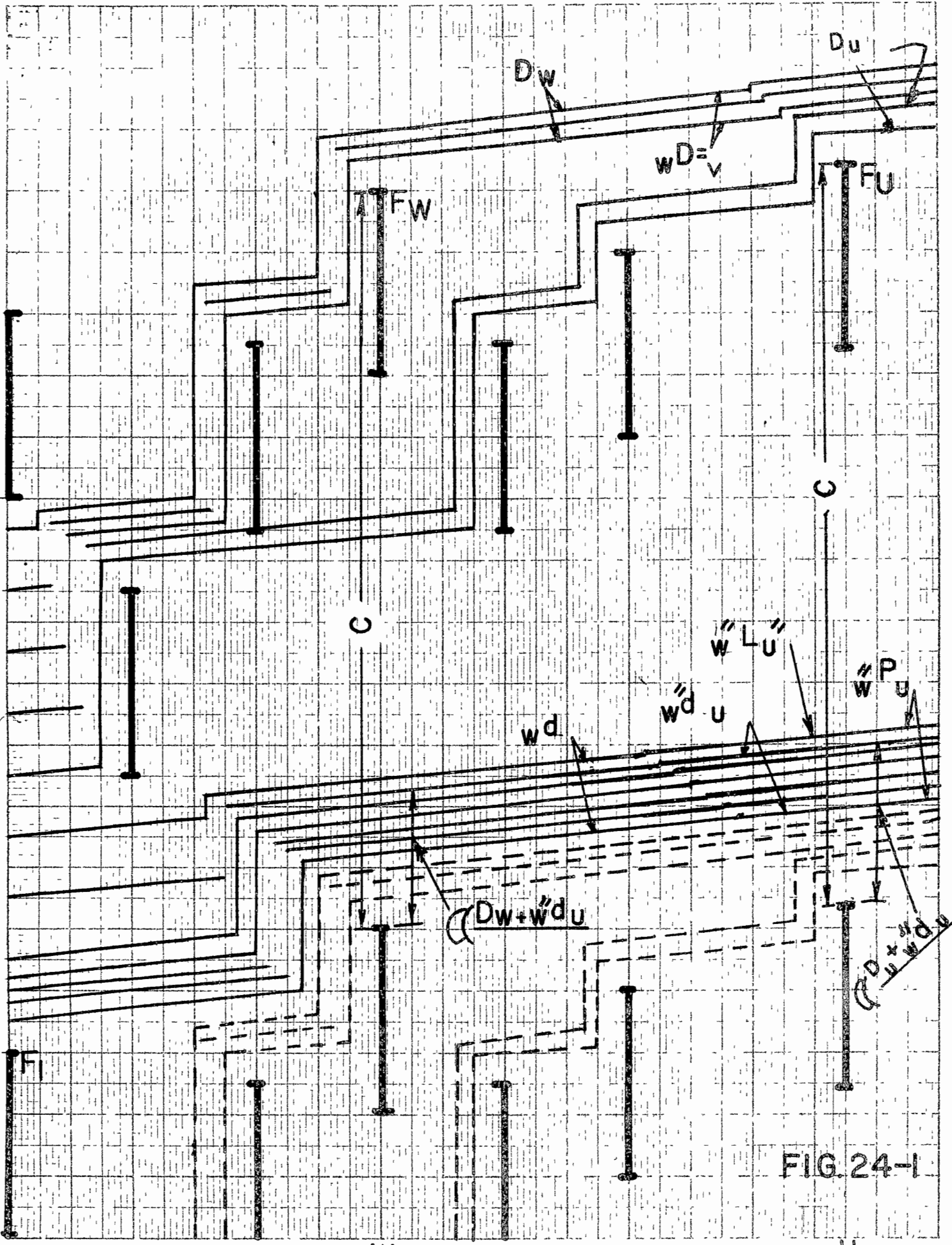


FIG. 24-1

I W U 3/4

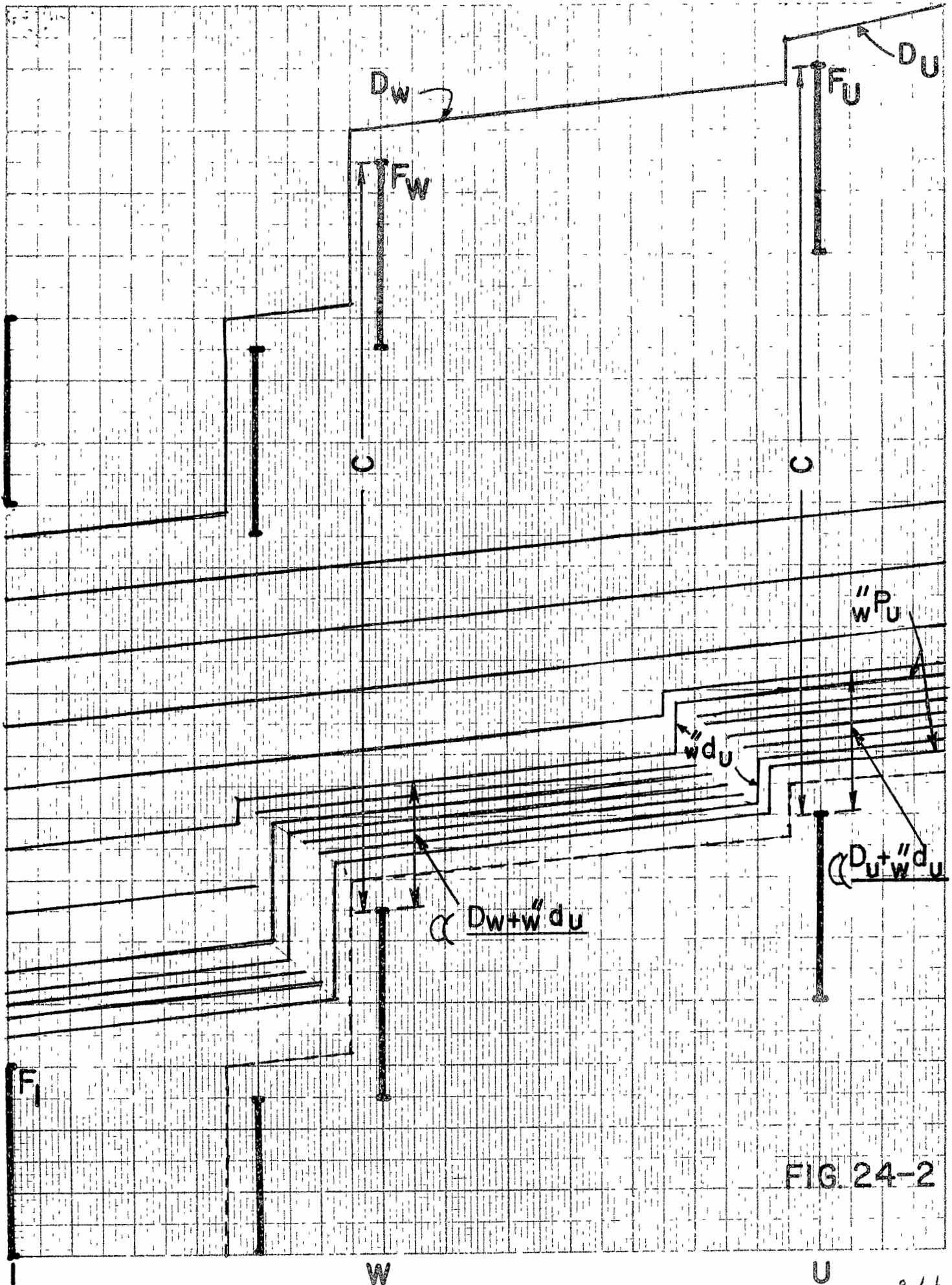


FIG. 24-2

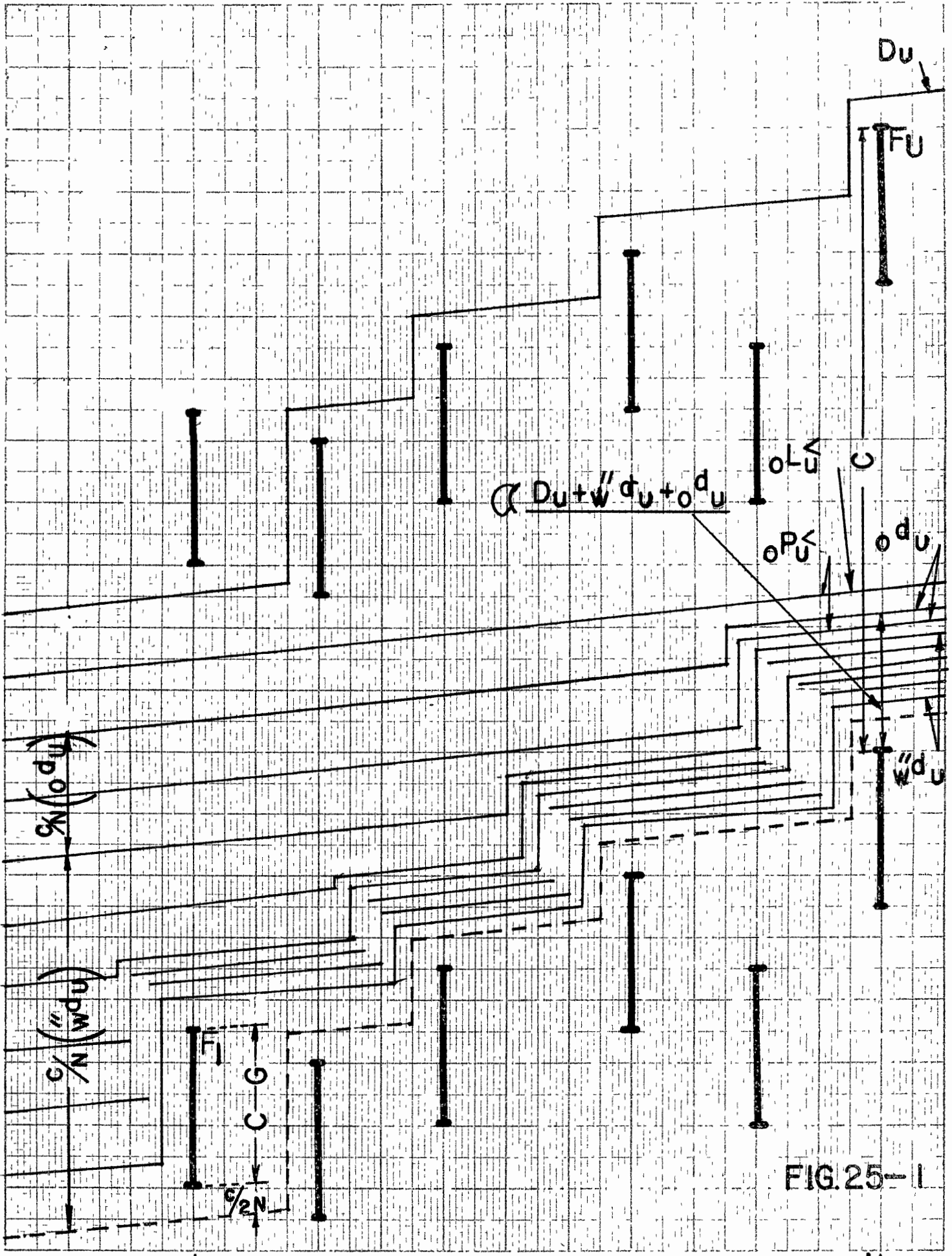


FIG. 25-1

1/2 INCH
 1/4 INCH
 1/8 INCH
 1/16 INCH

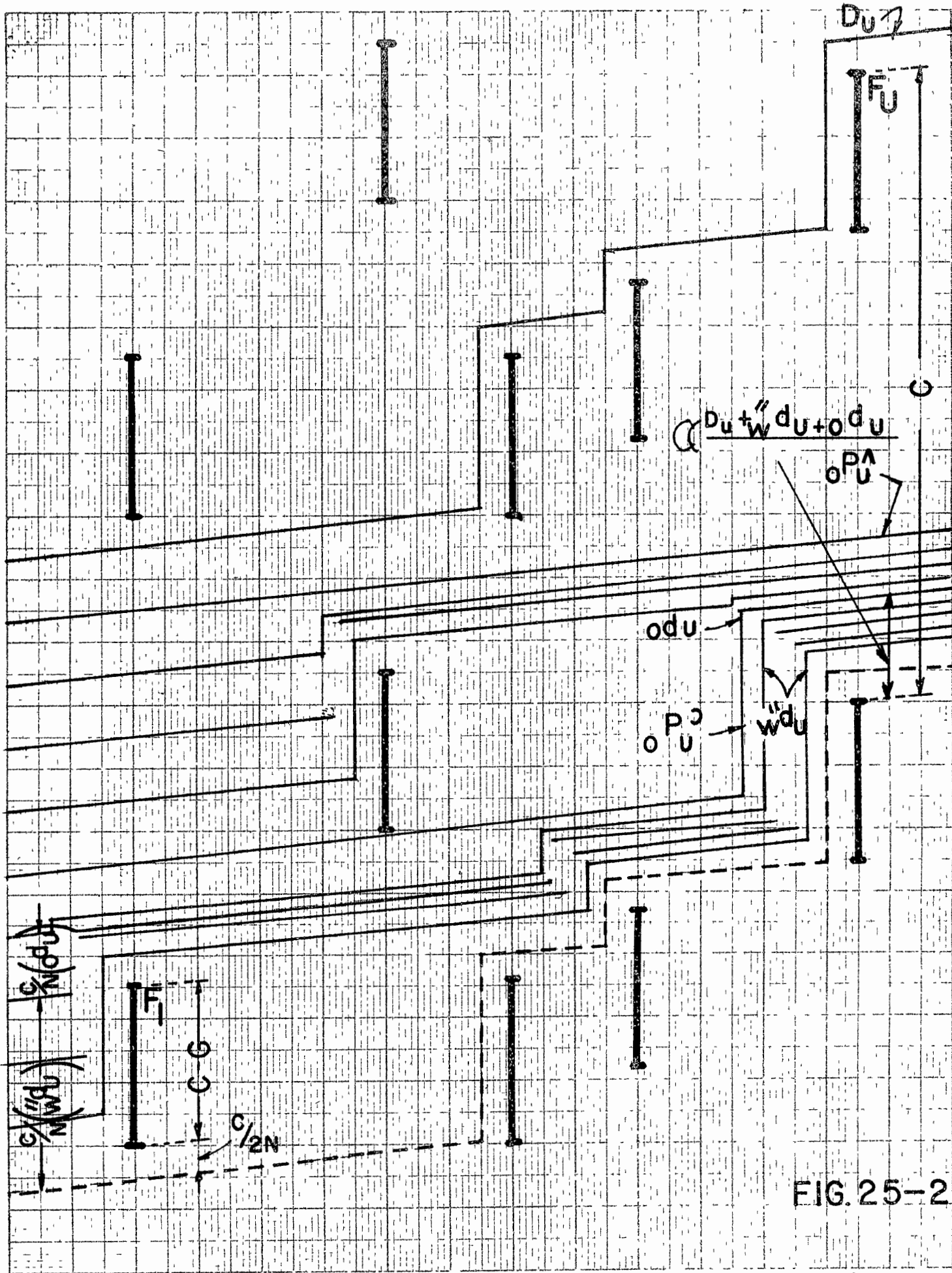


FIG. 25-2

U

